

Nonlinear Model Predictive Control

More than an introduction...

Mazen Alamir ¹

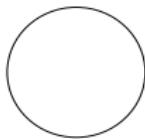
¹Laboratoire d'Automatique de Grenoble
CNRS-INPG-UJF, France.
mazen.alamir@inpg.fr

Atelier technique

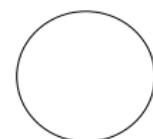
Regardless of the control strategy being used, the following keywords has to be addressed :

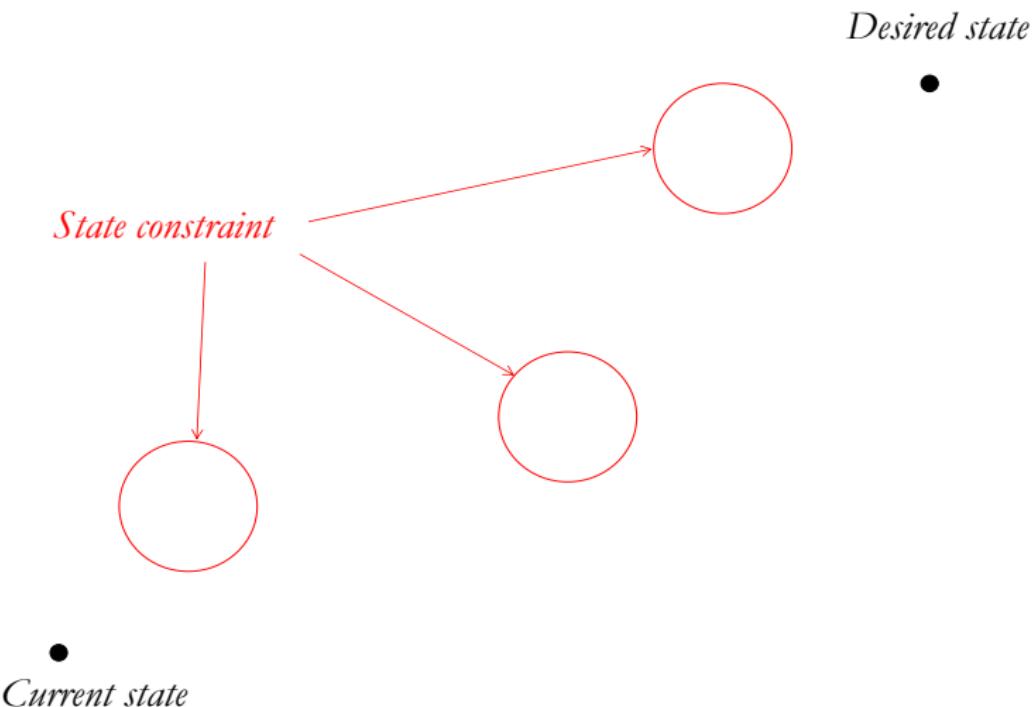
- **System model**
(State, control, measurement, disturbance)
- **Constraints**
(on state, control)
- **performance index**
(Operational cost, energy consumption, tracking quality)
- **Stability**
- **Robustness**

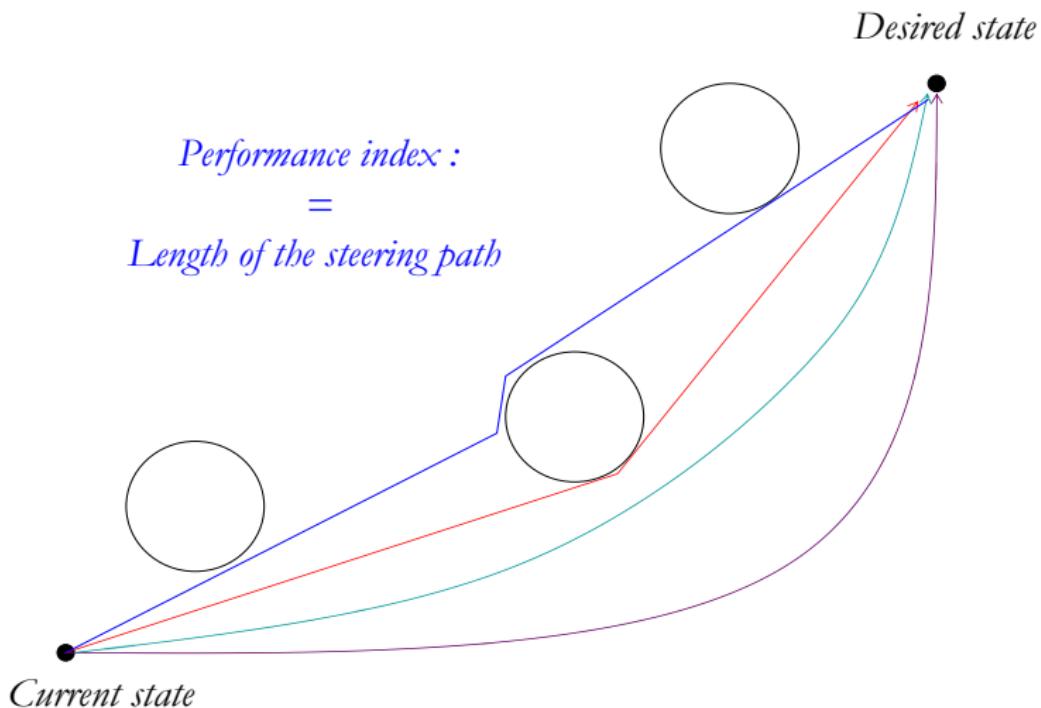
Current state

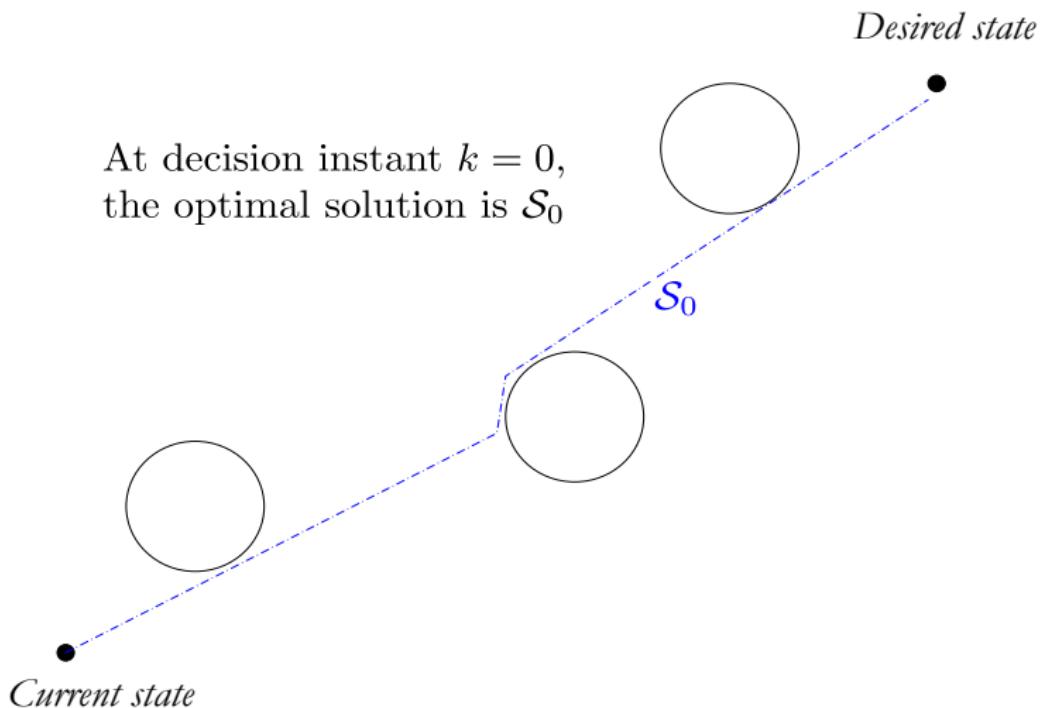


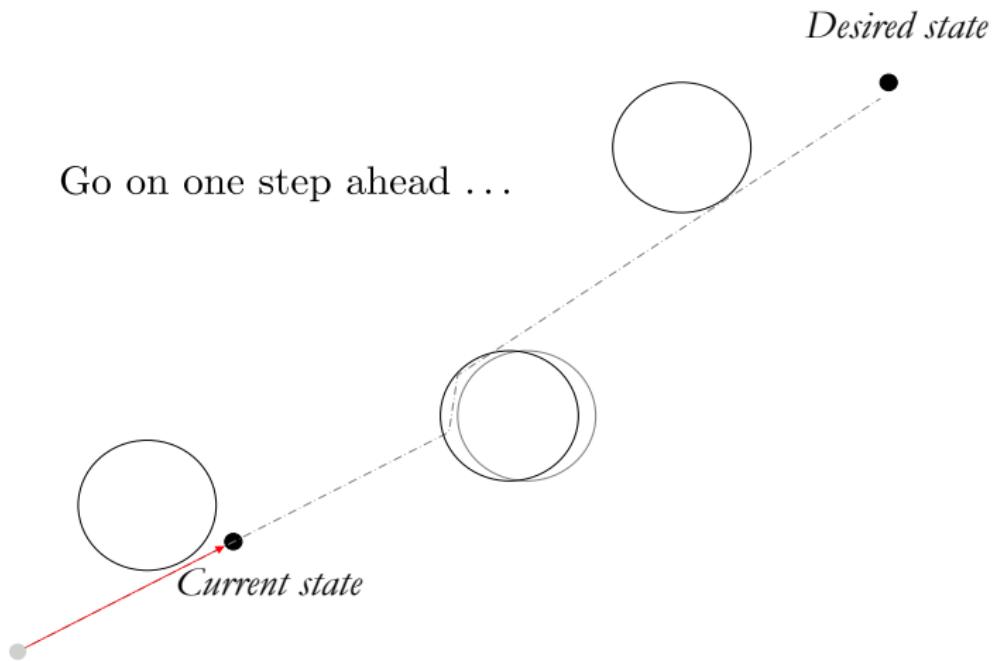
Desired state

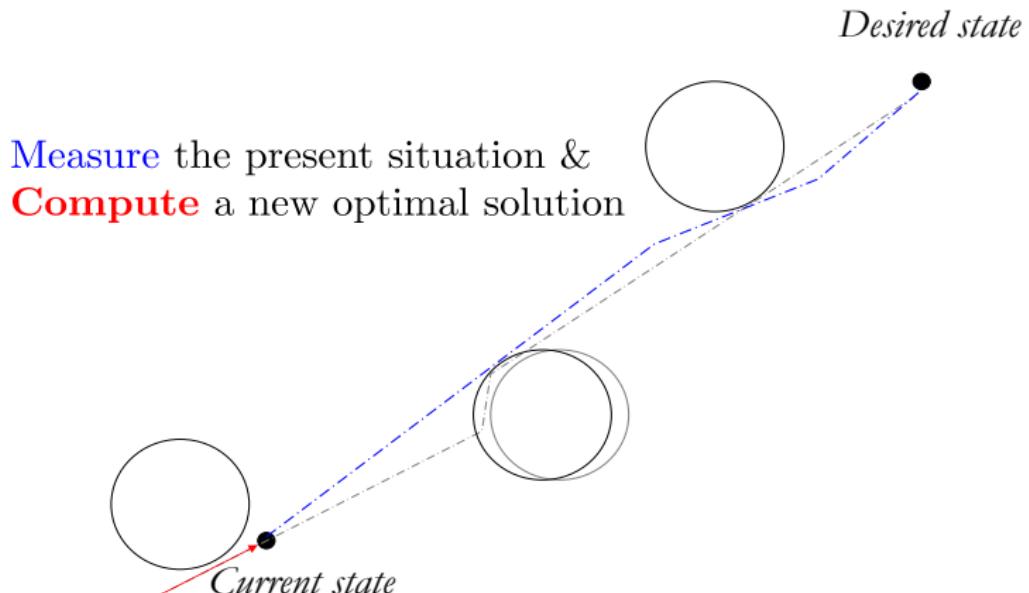


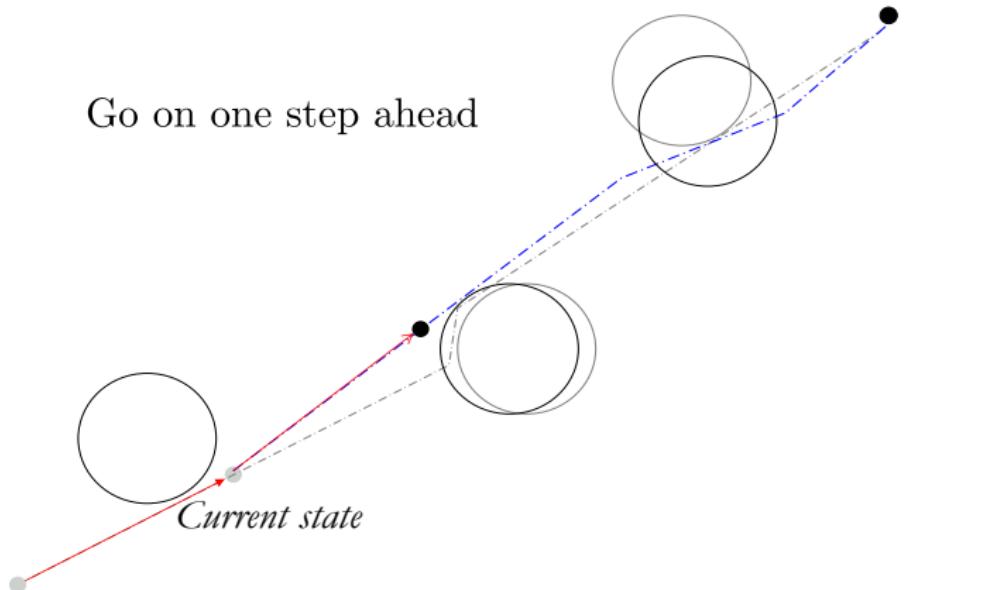




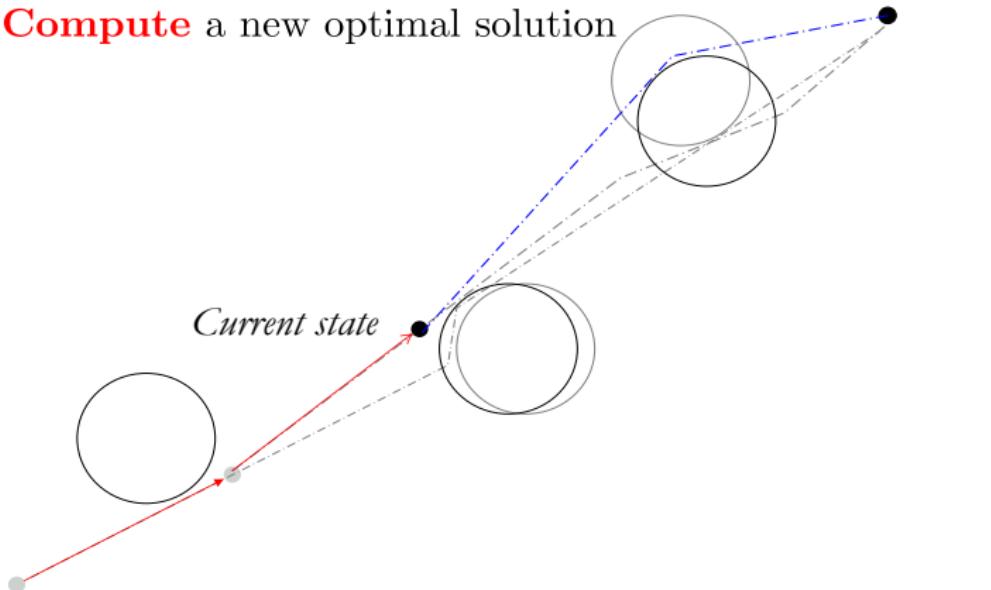


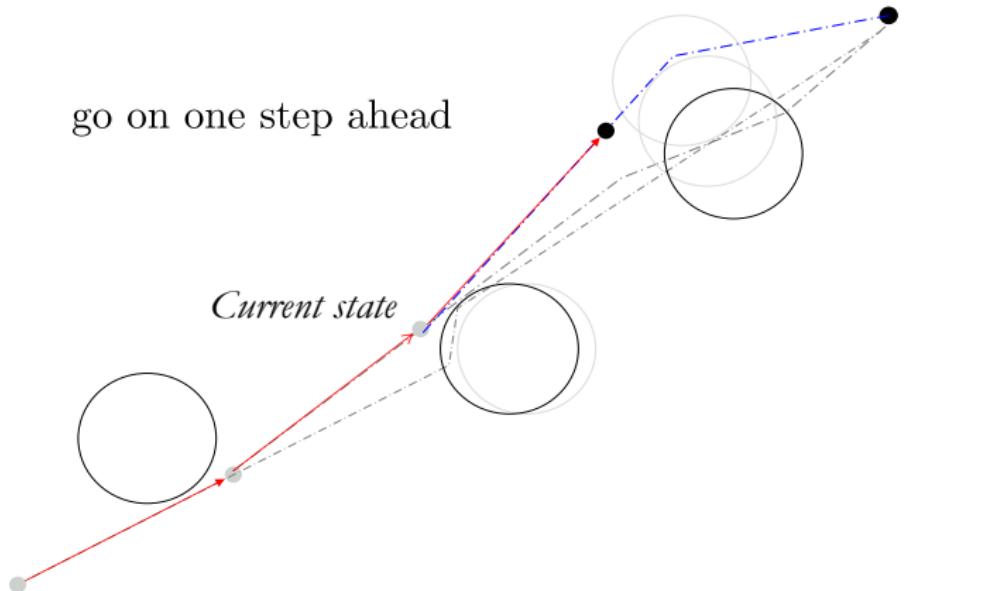




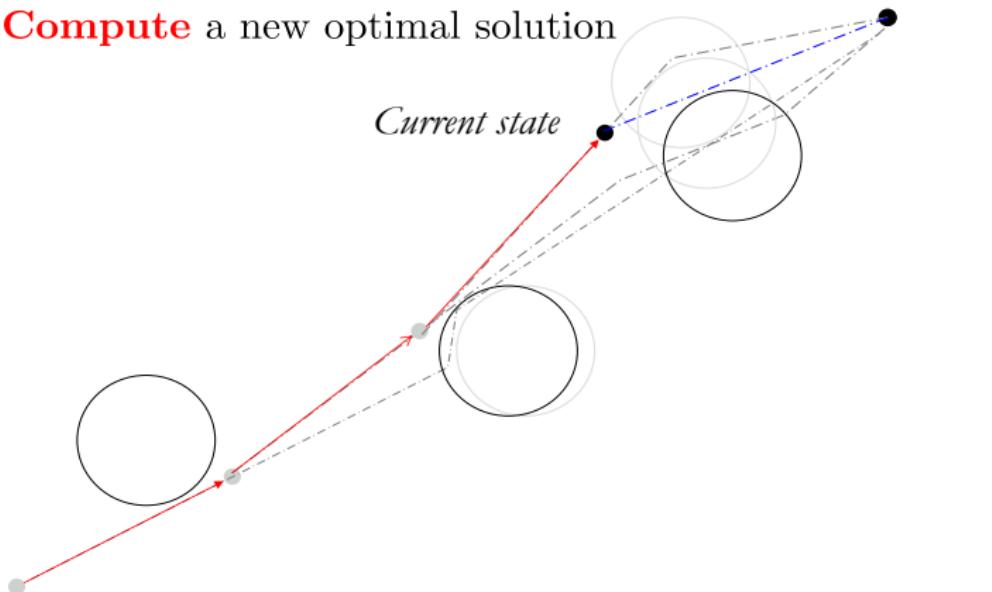


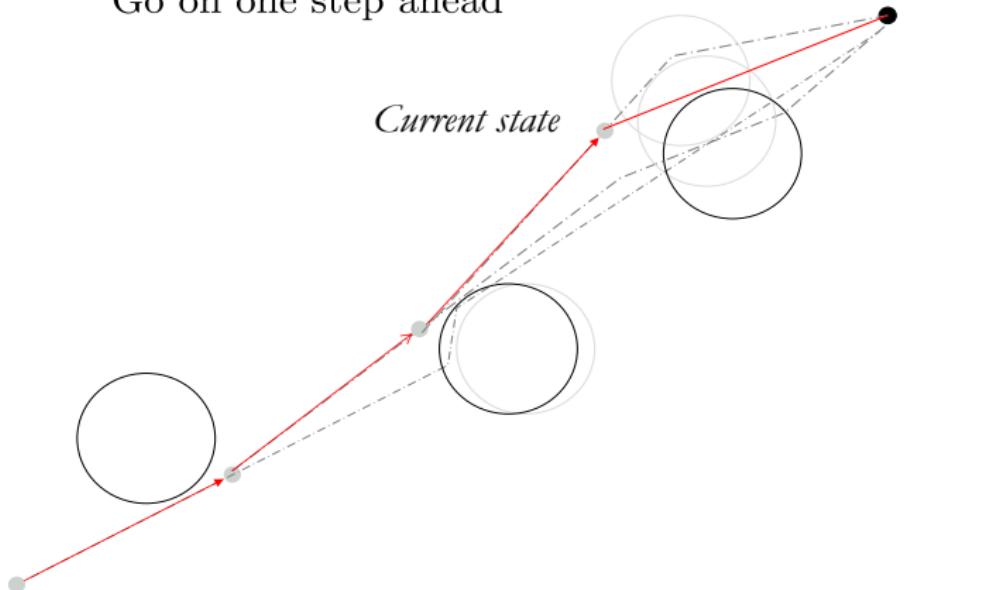
Measure the present situation &
Compute a new optimal solution

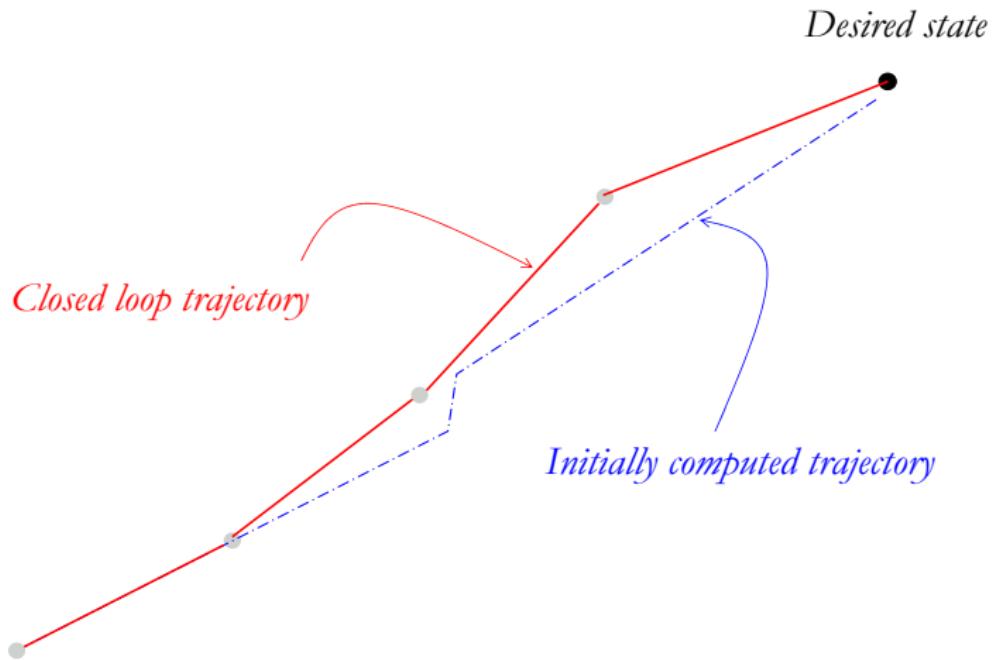




Measure the present situation &
Compute a new optimal solution







A simple feedback principle (informal)

- At each decision instant, evaluate the situation

A simple feedback principle (informal)

- At each decision instant, evaluate the situation
- Based on the evaluation, compute the best strategy

A simple feedback principle (informal)

- At each decision instant, evaluate the situation
- Based on the evaluation, compute the best strategy
- Apply the beginning of the strategy until the next decision instant

A simple feedback principle (informal)

- At each decision instant, evaluate the situation
- Based on the evaluation, compute the best strategy
- Apply the beginning of the strategy until the next decision instant
- Re-evaluate the situation

A simple feedback principle (informal)

- At each decision instant, evaluate the situation
- Based on the evaluation, compute the best strategy
- Apply the beginning of the strategy until the next decision instant
- Re-evaluate the situation
- Recompute the best strategy

A simple feedback principle (informal)

- At each decision instant, evaluate the situation
- Based on the evaluation, compute the best strategy
- Apply the beginning of the strategy until the next decision instant
- Re-evaluate the situation
- Recompute the best strategy
- Apply the first part until the next decision instant

A simple feedback principle (informal)

- At each decision instant, evaluate the situation
- Based on the evaluation, compute the best strategy
- Apply the beginning of the strategy until the next decision instant
- Re-evaluate the situation
- Recompute the best strategy
- Apply the first part until the next decision instant
- Keep doing

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$
- At decision instant $k+1$, measure the state $x(k+1)$

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$
- At decision instant $k+1$, measure the state $x(k+1)$
- Based on $x(k+1)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k+1)) := (u^0(k+1; x(k+1)) \quad u^0(k+2; x(k+1)) \quad \dots)$

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$
- At decision instant $k+1$, measure the state $x(k+1)$
- Based on $x(k+1)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k+1)) := (u^0(k+1; x(k+1)) \quad u^0(k+2; x(k+1)) \quad \dots)$
- Apply the control $u^0(k+1; x(k+1))$ on the sampling period $[k+1, k+2]$

A simple feedback principle (Formal)

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$
- At decision instant $k+1$, measure the state $x(k+1)$
- Based on $x(k+1)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k+1)) := (u^0(k+1; x(k+1)) \quad u^0(k+2; x(k+1)) \quad \dots)$
- Apply the control $u^0(k+1; x(k+1))$ on the sampling period $[k+1, k+2]$
- ...

A sampled state feedback

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \ u^0(k+1; x(k)) \ \dots \ u^0(k+i; x(k)) \ \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$
- At decision instant $k+1$, measure the state $x(k+1)$
- Based on $x(k+1)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k+1)) := (u^0(k+1; x(k+1)) \ u^0(k+2; x(k+1)) \ \dots)$
- Apply the control $u^0(k+1; x(k+1))$ on the sampling period $[k+1, k+2]$
- ...

A sampled state feedback

- **At decision instant k** , measure the state $x(k)$
- Based on $x(k)$, compute the best sequence of actions :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- **Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$**

A state feedback

We have defined a sampled state feedback

$$u(k) = u^0(k; x(k))$$

A key task . . .

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, **compute the best sequence of actions** :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$
- At decision instant $k+1$, measure the state $x(k+1)$
- Based on $x(k+1)$, **compute the best sequence of actions** :
 $\mathbf{u}^0(x(k+1)) := (u^0(k+1; x(k+1)) \quad u^0(k+2; x(k+1)) \quad \dots)$
- Apply the control $u^0(k+1; x(k+1))$ on the sampling period $[k+1, k+2]$
- ...

A key task . . .

- At decision instant k , measure the state $x(k)$
- Based on $x(k)$, **compute the best sequence of actions** :
 $\mathbf{u}^0(x(k)) := (u^0(k; x(k)) \quad u^0(k+1; x(k)) \quad \dots \quad u^0(k+i; x(k)) \quad \dots)$
- Apply the control $u^0(k; x(k))$ on the sampling period $[k, k+1]$

We need an optimization problem

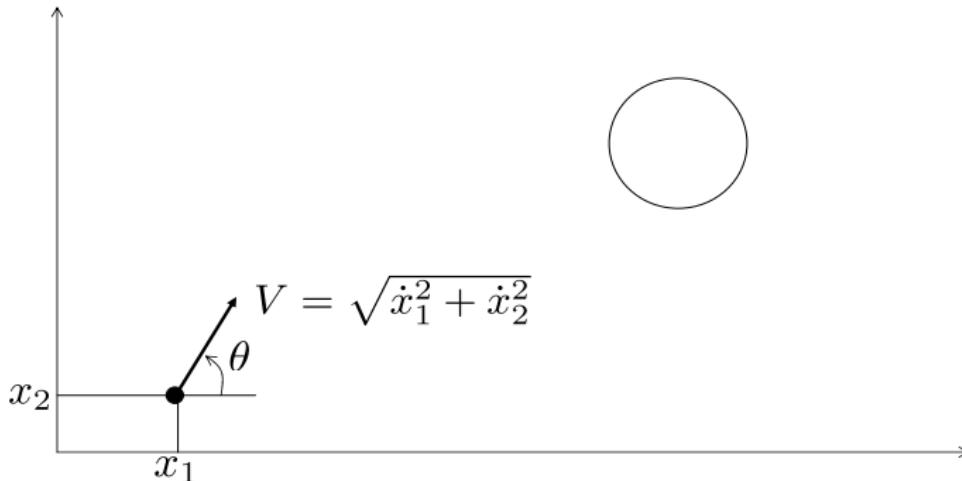
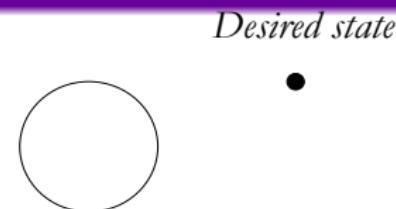
$$\mathcal{P}(x(k)) \quad : \quad \min_{\mathbf{u}} \left\{ V(x(k), \mathbf{u}) \quad | \quad \mathbf{u} \in \mathcal{U}(x(k)) \right\}$$

$\mathbf{u}^0(x(k))$ is A solution of $\mathcal{P}(x(k))$

How to define & Solve $\mathcal{P}(x)$ for our example ?

Step 1 : Write down the system model

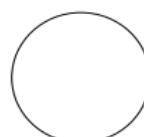
State of the system : $x = \begin{pmatrix} x_1 \\ x_2 \\ \theta \\ V \end{pmatrix}$



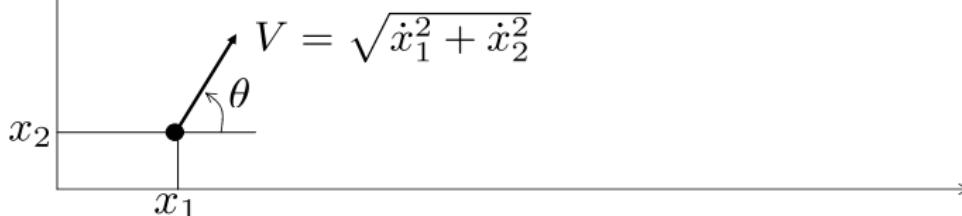
Step 1 : Write down the system model

State of the system : $x = \begin{pmatrix} x_1 \\ x_2 \\ \theta \\ V \end{pmatrix}$

Desired state



$$\boxed{\begin{aligned}\dot{x}_1 &= x_4 \cos(x_3) \\ \dot{x}_2 &= x_4 \sin(x_3) \\ \dot{x}_3 &= u_1 \\ \dot{x}_4 &= u_2\end{aligned}}$$



Step 1 : Write down the system model

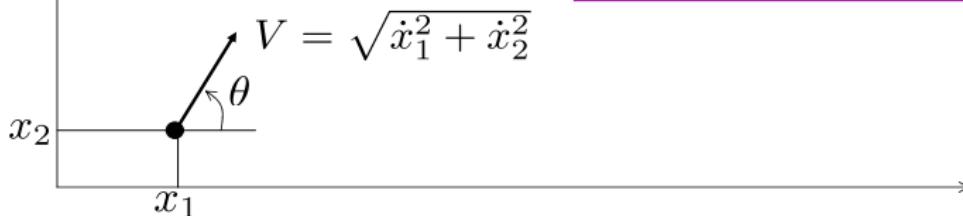
State of the system : $x = \begin{pmatrix} x_1 \\ x_2 \\ \theta \\ V \end{pmatrix}$

$$\begin{aligned}\dot{x}_1 &= x_4 \cos(x_3) \\ \dot{x}_2 &= x_4 \sin(x_3) \\ \dot{x}_3 &= u_1 \\ \dot{x}_4 &= u_2\end{aligned}$$

```

function xdot=car(t,x)
    global u_glob
    xdot=zeros(4,1);
    xdot(1)=x(4)*cos(x(3));
    xdot(2)=x(4)*sin(x(3));
    xdot(3)=u_glob(1);
    xdot(4)=u_glob(2);
return

```



Step 2 : Obtain the sampled-time model

Given the continuous system

$$\dot{x} = f_c(x, u)$$

Compute the implicit τ -discrete dynamics

$$x^+(k) = x(k+1) = f(x(k), u(k))$$

where $x(k+1)$ is the solution at instant τ of

$$\dot{\xi} = f_c(\xi, u(k)) \quad ; \quad \xi(0) = x(k)$$

```
function xdot=car(t,x)
    global u_glob
    xdot=zeros(4,1);
    xdot(1)=x(4)*cos(x(3));
    xdot(2)=x(4)*sin(x(3));
    xdot(3)=u_glob(1);
    xdot(4)=u_glob(2);
return
```

Continuous system

```
function xplus=car_d(x,u,tau)
    global u_glob
    u_glob=u;
    [tt,xx]=ode45(@car,[0,tau],x);
    xplus=xx(end,:)';
return
```

τ -sampled system

Some notations before we continue

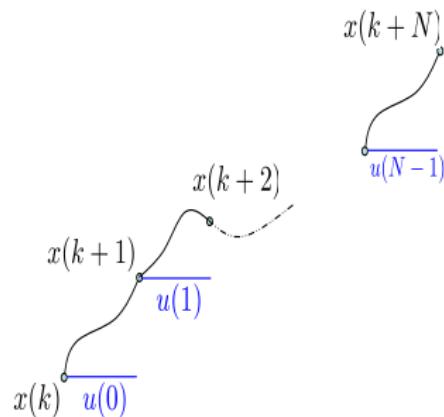
Consider

$$x^+ = f(x, u)$$

$$\mathbf{u} := (u(0), u(1), \dots, u(N-1))$$

Notation

$$x^{\mathbf{u}}(\cdot, x(k)) := \left\{ x(k+i) \right\}_{i=0}^N$$



$$x(k+i) = f(x(k+i-1), u(i-1))$$

Recall

$$\begin{aligned}\mathcal{P}(x(k)) & : \min_{\mathbf{u}} \left\{ V(x(k), \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x(k)) \right\} \\ \mathbf{u}^0(x(k)) & \text{ is A solution of } \mathcal{P}(x(k))\end{aligned}$$

Step 3 : Write down the constraints

Step 3 : Write down the constraints

The final constraint

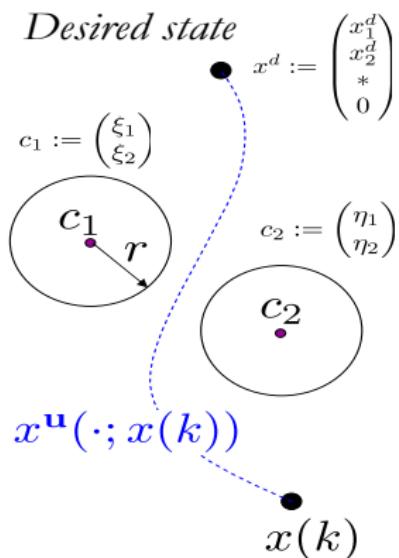
$$x^{\mathbf{u}}(N; x(k)) - x^d = 0$$

Obstacle avoidance

$$r - \min_{i \in \{1,2\}} d(x^{\mathbf{u}}(\cdot; x(k)), c_i) \leq 0$$

Saturation constrainte

$$\mathbf{u} \in [u_{min}, u_{max}]^N$$



Step 3 : Write down the constraints

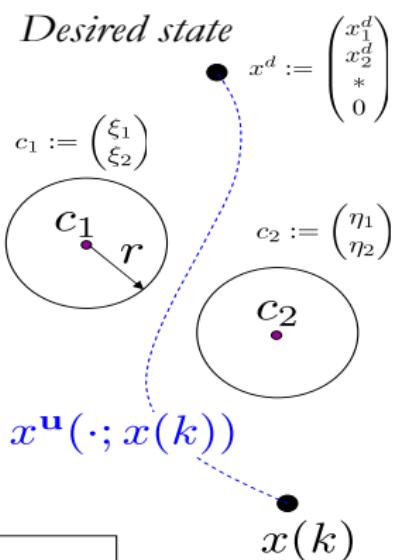
Equality constraints

$$G_1(\mathbf{u}, x(k)) = 0$$

Inequality constraints

$$G_2(\mathbf{u}, x(k)) \leq 0$$

$$\mathcal{U}(x(k)) := \left\{ \mathbf{u} \mid G_1 = 0 \text{ and } G_2 \leq 0 \right\}$$



Step 3 : Write down the constraints

```
function [G1,G2]=constraintes(les_u,x,tau)
    global xd xi eta u_min u_max
    N=length(les_u(:,1));
    xu=zeros(N,4); xu(1,:)=x';
    d(1)=min(norm(xu(1,1:2)-xi),norm(xu(1,1:2)-eta));
    for i=2:N,
        xu(i,:)=car_d(xu(i-1,:)',lesu(i-1,:)',tau);
        d(i)=min(norm(xu(i,1:2)-xi),norm(xu(i,1:2)-eta));
    end
    cond_min=max(max(ones(N,1)*u_min'-lesu));
    cond_max=max(max(lesu-ones(N,1)*u_max'));
    G1=xu(N,:)'-xd;
    G2=[r-min(d);cond_min;cond_max];
return
```

Recall

$$\begin{aligned}\mathcal{P}(x(k)) & : \min_{\mathbf{u}} \left\{ V(x(k), \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x(k)) \right\} \\ \mathbf{u}^0(x(k)) & \text{ is A solution of } \mathcal{P}(x(k))\end{aligned}$$

Write down the performance index

$$V(x(k), \mathbf{u}) := \sum_{i=1}^N \|x^{\mathbf{u}}(i; x(k)) - x^d\|^2$$

Write down the performance index

$$V(x(k), \mathbf{u}) := \sum_{i=1}^N \|x^{\mathbf{u}}(i; x(k)) - x^d\|^2$$

```
function f=cost(lesu,x,tau)
    global xd
    N=length(les_u(:,1));
    xu=zeros(N,4);
    xu(1,:)=x';
    f = 0;
    for i=2:N,
        xu(i,:)=car_d(xu(i-1,:)',lesu(i-1,:)',tau);
        f = f+norm(xu(i,:)'-xd)^2;
    end
    return
```

26/10/05 00:00

MATLAB Command Window

1 of 1

FMINCON finds a constrained minimum of a function of several variables.

FMINCON attempts to solve problems of the form:

```
min F(X)  subject to: A*X <= B, Aeq*X = Beq (linear constraints)
X           C(X) <= 0, Ceq(X) = 0   (nonlinear constraints)
LB <= X <= UB
```

X=FMINCON(FUN,X0,A,B) starts at X0 and finds a minimum X to the function FUN, subject to the linear inequalities $A*X \leq B$. FUN accepts input X and returns a scalar function value F evaluated at X. X0 may be a scalar, vector, or matrix.

X=FMINCON(FUN,X0,A,B,Aeq,Beq) minimizes FUN subject to the linear equalities $Aeq*X = Beq$ as well as $A*X \leq B$. (Set A=[] and B=[] if no inequalities exist.)

X=FMINCON(FUN,X0,A,B,Aeq,Beq,lb,ub) defines a set of lower and upper bounds on the design variables, X, so that a solution is found in the range $lb \leq X \leq ub$. Use empty matrices for LB and UB if no bounds exist. Set $lb(i) = -\infty$ if $X(i)$ is unbounded below; set $ub(i) = \infty$ if $X(i)$ is unbounded above.

X=FMINCON(FUN,X0,A,B,Aeq,Beq,lb,ub,nonlcon) subjects the minimization to the constraints defined in NONLCON. The function NONLCON accepts X and returns the vectors C and Ceq, representing the nonlinear inequalities and equalities respectively. FMINCON minimizes FUN such that $C(X) \leq 0$ and $Ceq(X) = 0$. (Set LB=[] and/or UB=[] if no bounds exist.)



Coming next ...

- Existence of solutions
- Closed-loop stability

Existence of solutions

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \quad | \quad \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \quad | \quad \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

in which \mathbb{U} compact ; \mathbb{X} compact ; $X_f = \{x^d\} \subset \mathbb{X}$ closed.

Existence of solutions

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \quad | \quad \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \quad | \quad \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

in which \mathbb{U} compact ; \mathbb{X} compact ; $X_f = \{x^d\} \subset \mathbb{X}$ closed.

No global definition under bounded control

one must have $x \in X_N$ the subset of states from which X_f is accessible by N -step controls in \mathbb{U} and trajectories in \mathbb{X} .

Existence of solutions

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

in which \mathbb{U} compact ; \mathbb{X} compact ; $X_f = \{x^d\} \subset \mathbb{X}$ closed.

for all $x \in X_N$, main arguments

$V(x, \cdot)$ is continuous and $\mathcal{U}(x)$ is compact.

Close-loop stability

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

$$x^d = 0 \quad ; \quad X_f = \{0\} \quad ; \quad f(0, 0) = 0$$

Close-loop stability

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

$$x^d = 0 \quad ; \quad X_f = \{0\} \quad ; \quad f(0, 0) = 0$$

An optimal solution :

$$\mathbf{u}^0(x) := (u^0(0; x) \ u^0(1; x) \ \dots \ u^0(N - 1; x)) \in \mathbb{U}^N$$

Close-loop stability

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

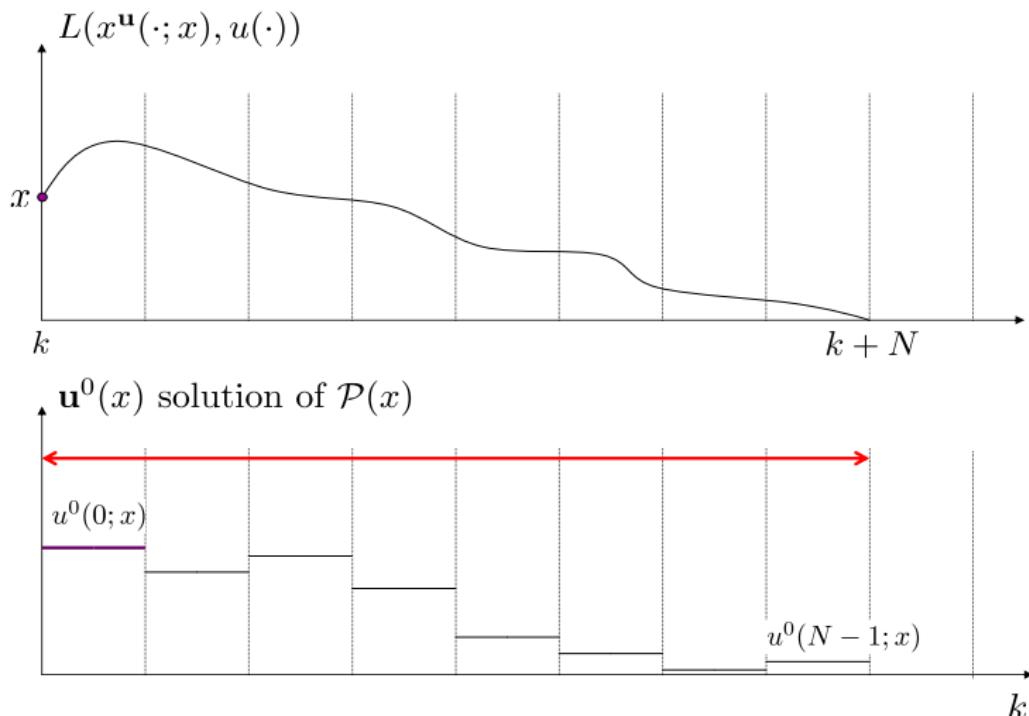
$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

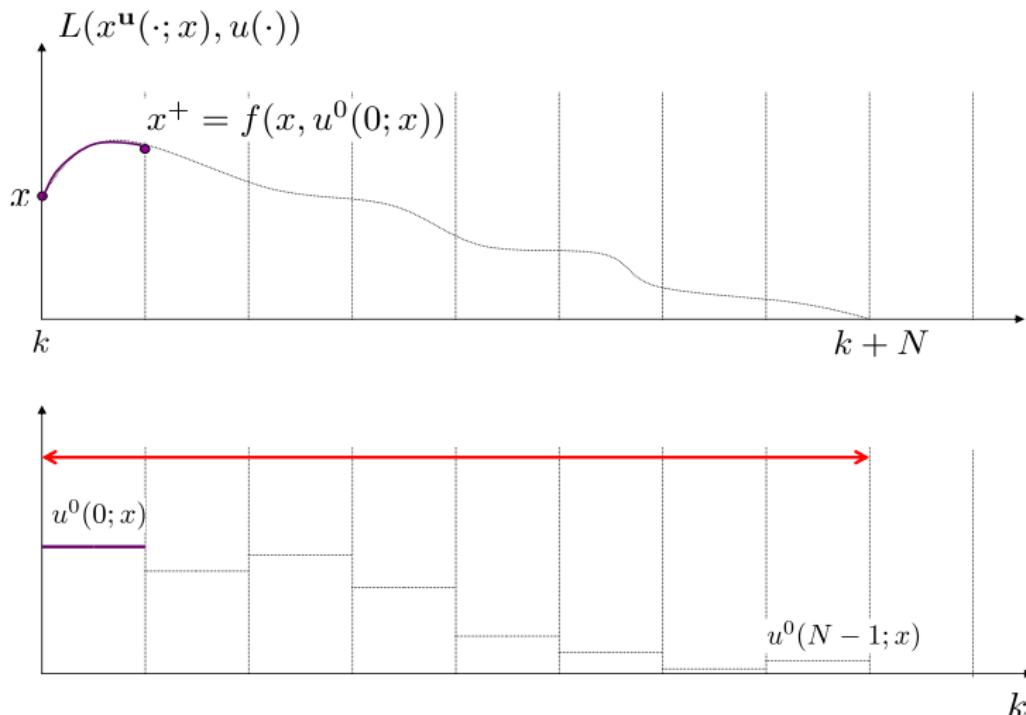
$$x^d = 0 \quad ; \quad X_f = \{0\} \quad ; \quad f(0, 0) = 0$$

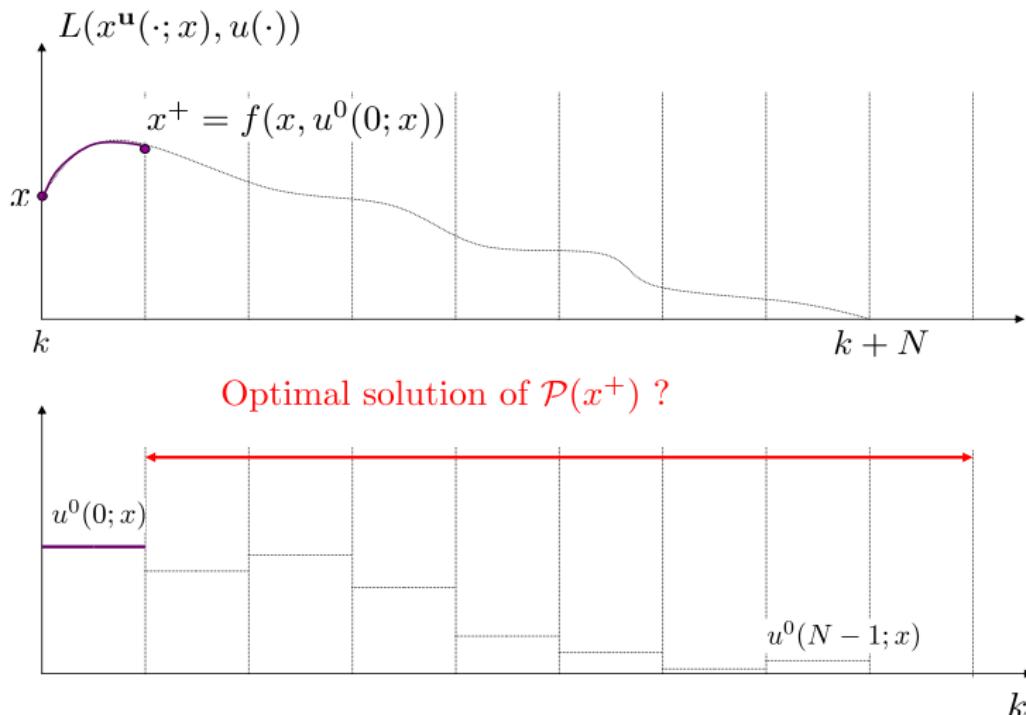
An optimal solution :

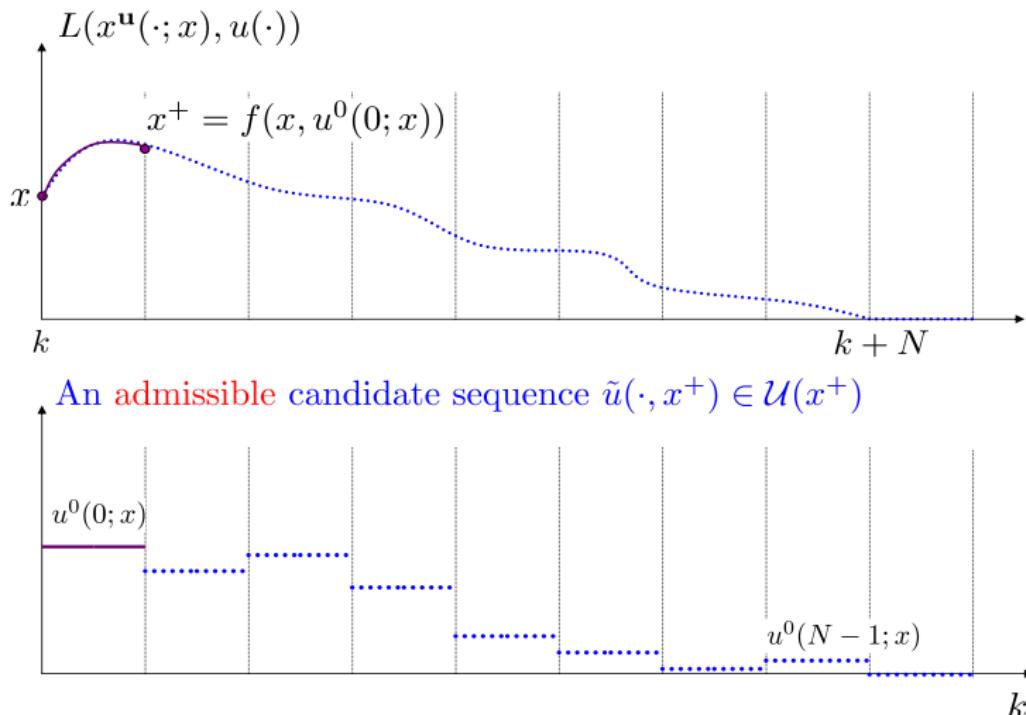
$$\mathbf{u}^0(x) := (u^0(0; x) \ u^0(1; x) \ \dots \ u^0(N - 1; x)) \in \mathbb{U}^N$$

Sampled state feedback : $\kappa^0(x) := u^0(0; x)$

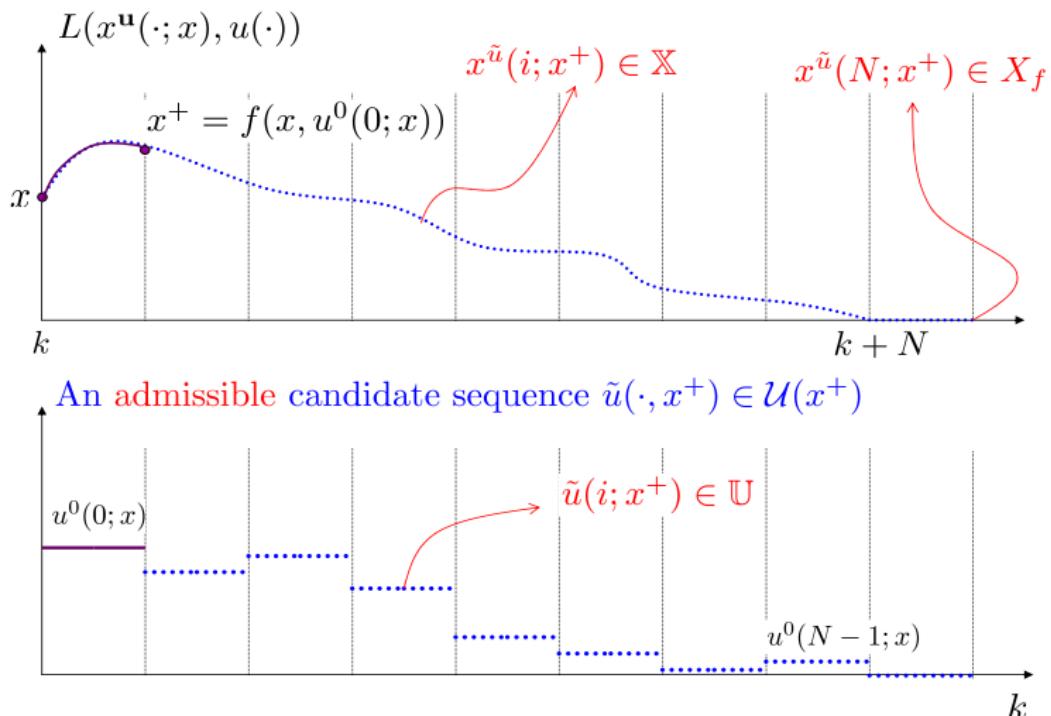


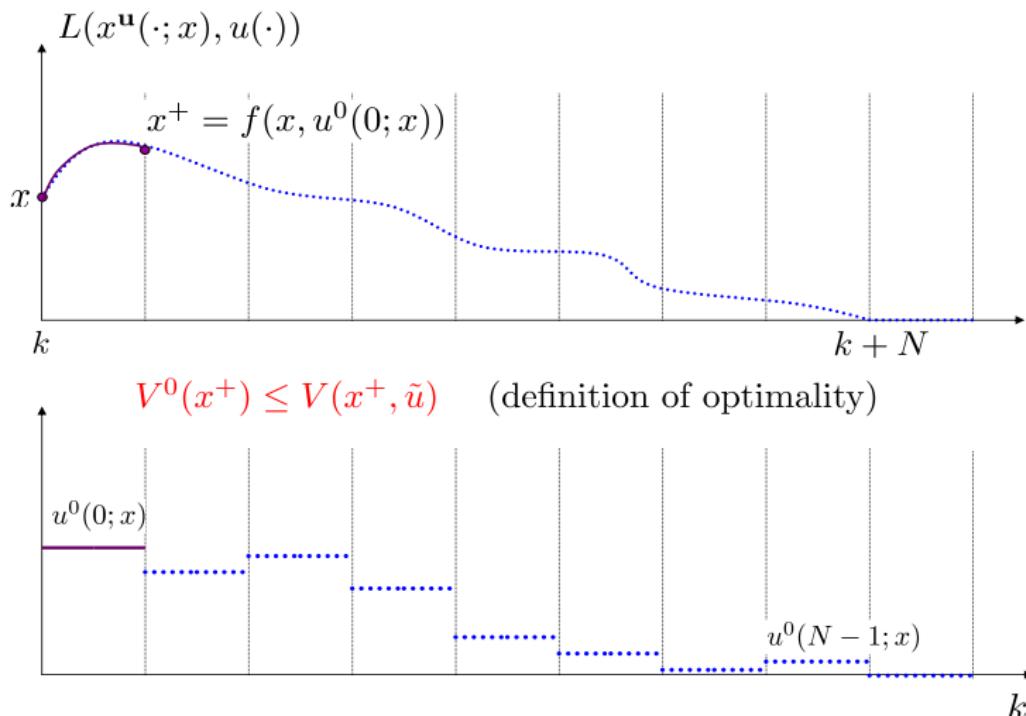


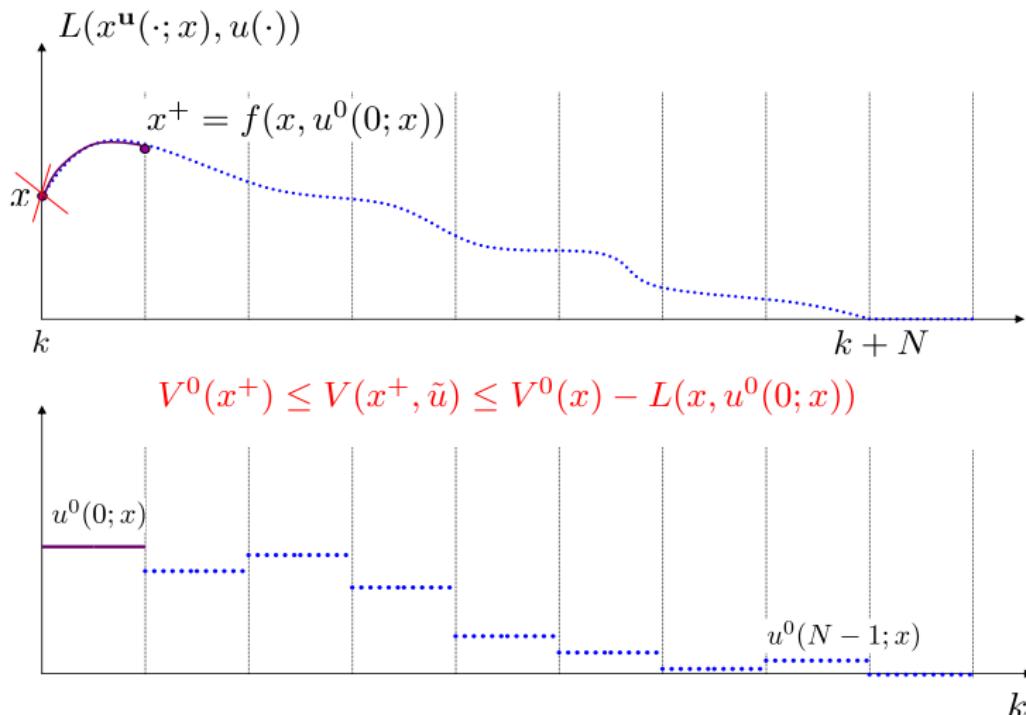




An admissible candidate sequence $\tilde{u}(\cdot, x^+) \in \mathcal{U}(x^+)$







Closed loop stability

Therefore, on the closed loop trajectory :

$$V^0(x(k+1)) \leq V^0(x(k)) - L(x(k), \kappa^0(x(k)))$$

therefore,

$$\lim_{k \rightarrow \infty} L(x(k), \kappa^0(x(k))) = 0$$

Consequently, if $L(\cdot, \cdot)$ is a **continuous positive definite function in x** , one has

$$\lim_{k \rightarrow \infty} x(k) = 0$$

Close-loop stability

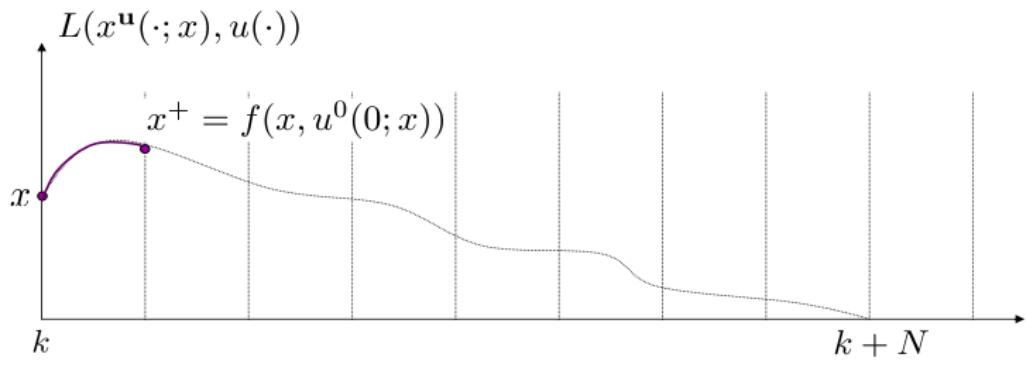
$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\}$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

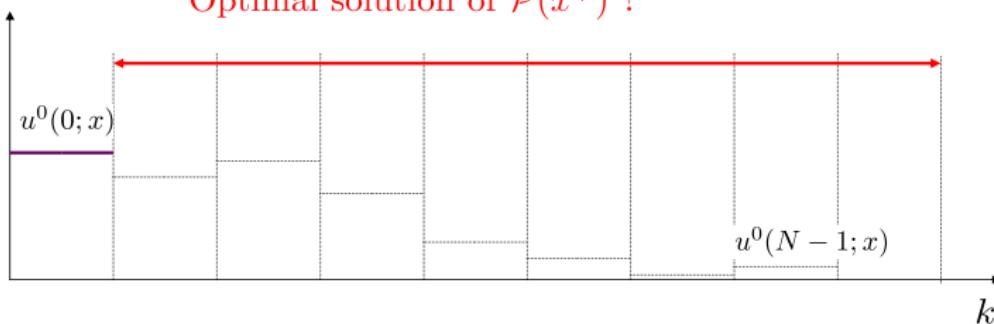
$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

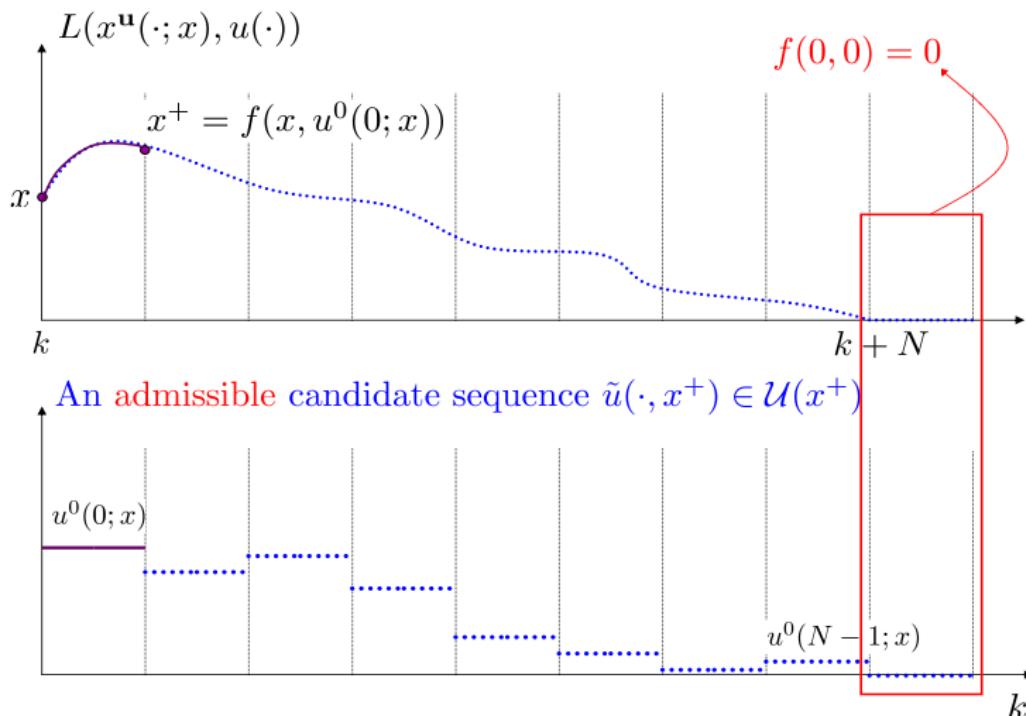
$$x^d = 0 \quad ; \quad X_f = \{0\} \quad ; \quad f(0, 0) = 0$$

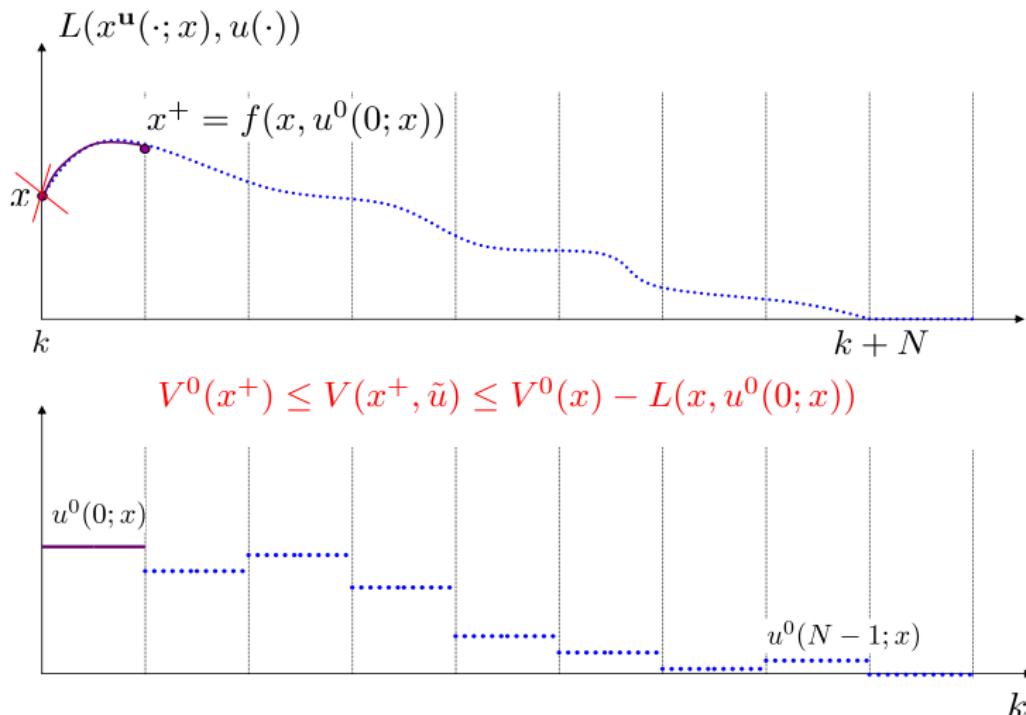
The final equality constraint : A key role

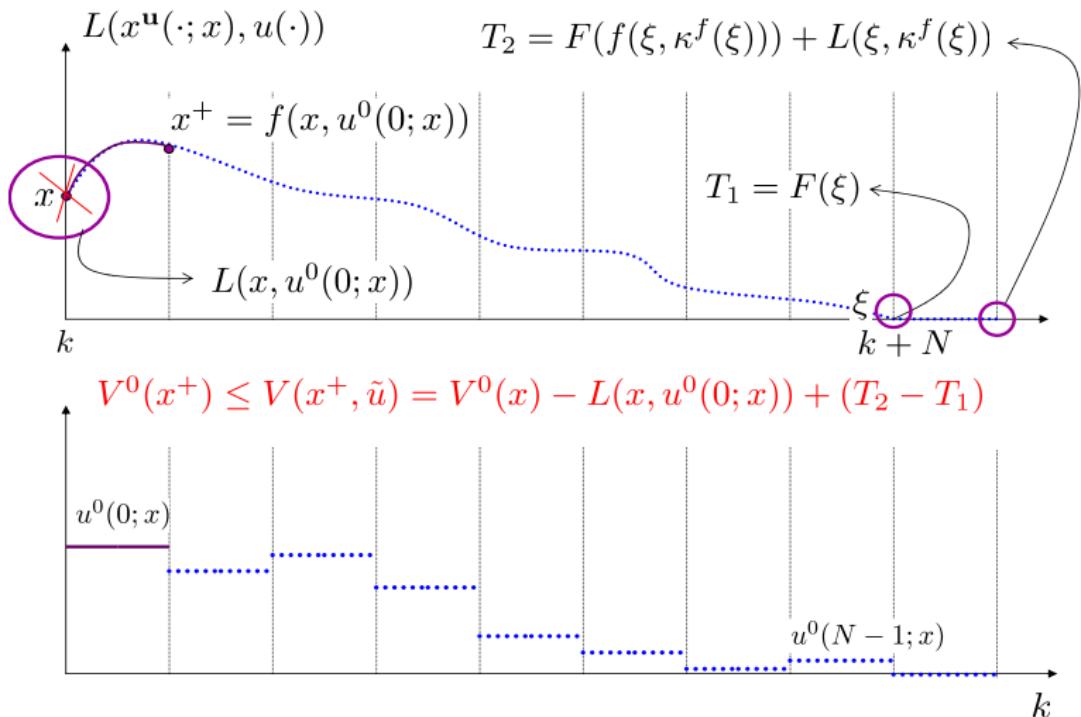


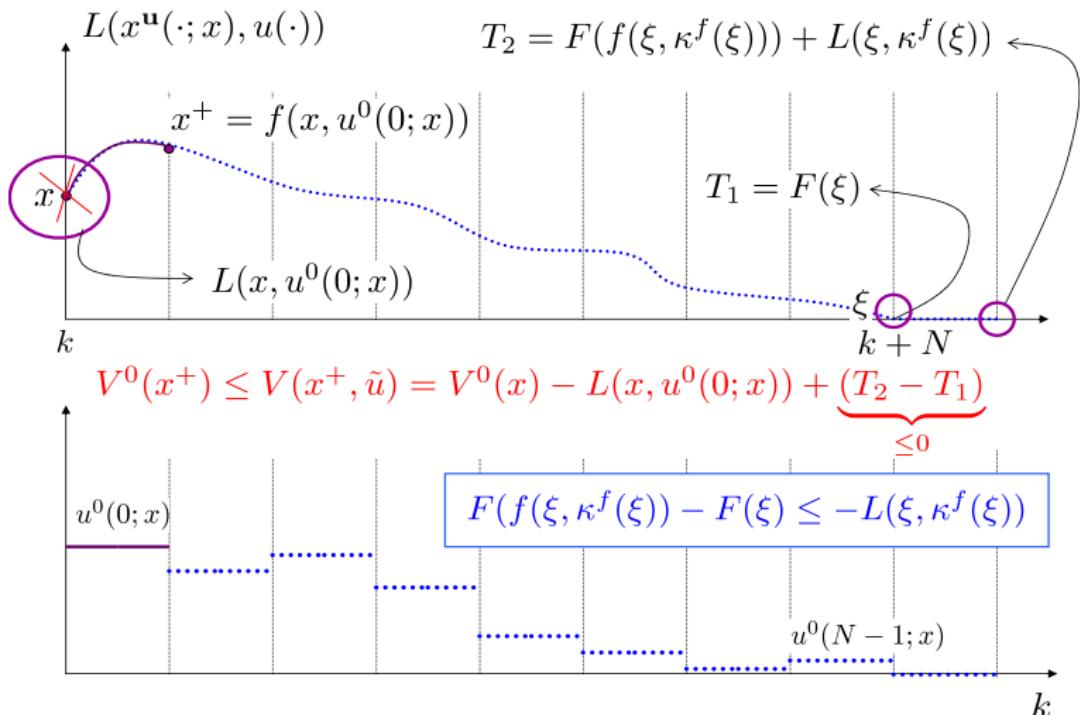
Optimal solution of $\mathcal{P}(x^+) ?$











First useful property of $X_f = \{0\}$

For all $\xi \in X_f$, there exists an admissible control $\kappa^f(\xi)$ such that :

$$f(\xi, \kappa^f(\xi)) \in X_f$$

(X_f is positively invariant under $\kappa^f(\cdot)$)

Second useful property of $X_f = \{0\}$

For all $\xi \in X_f$, the admissible control $\kappa^f(\xi)$ is such that :

$$F(f(\xi, \kappa^f(\xi))) - F(\xi) \leq -L(\xi, \kappa^f(\xi))$$

(The terminal cost $F(\cdot)$ is a Lyapunov function for the closed loop dynamics under $\kappa^f(\cdot)$)

Necessary conditions for well defined and stable NMPC scheme

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u)$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

Necessary conditions for well defined and stable NMPC scheme

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u)$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

Condition 1 : Continuity

The applications f, F, L are continuous in their arguments.

Necessary conditions for well defined and stable NMPC scheme

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u)$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

Condition 2 : Compactness

- ✓ \mathbb{U} is compact
- ✓ \mathbb{X} and $X_f \subset \mathbb{X}$ are closed.

Necessary conditions for well defined and stable NMPC scheme

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u)$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

Condition 3 : Detectability

The integral cost L must be such that

$$\left\{ L(x, u) \rightarrow 0 \right\} \Rightarrow \left\{ x \rightarrow 0 \right\}$$

Necessary conditions for well defined and stable NMPC scheme

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u)$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

Condition 4 : X_f is positively invariant under some local $\kappa^f(\cdot)$

For all $\xi \in X_f$, there exists an admissible control $\kappa^f(\xi)$ such that :

$$f(\xi, \kappa^f(\xi)) \in X_f$$

Necessary conditions for well defined and stable NMPC scheme

$$\begin{aligned}\mathcal{P}(x) &: \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u) \\ \mathcal{U}(x) &:= \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\} \\ V(x, \mathbf{u}) &= F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))\end{aligned}$$

Condition 5 : The terminal cost $F(\cdot)$ is a Lyapunov under $\kappa^f(\cdot)$

For all $\xi \in X_f$, the admissible control $\kappa^f(\xi)$ is such that :

$$F(f(\xi, \kappa^f(\xi))) - F(\xi) \leq -L(\xi, \kappa^f(\xi))$$

Necessary conditions for well defined and stable NMPC scheme

$$\mathcal{P}(x) : \min_{\mathbf{u}} \left\{ V(x, \mathbf{u}) \mid \mathbf{u} \in \mathcal{U}(x) \right\} ; \quad x^+ = f(x, u)$$

$$\mathcal{U}(x) := \left\{ \mathbf{u} \in \mathbb{U}^N \mid \forall i \quad x^{\mathbf{u}}(i; x) \in \mathbb{X} \quad \text{and} \quad x^{\mathbf{u}}(N, x) \in X_f \right\}$$

$$V(x, \mathbf{u}) = F(x(N; x)) + \sum_{i=0}^N L(x^{\mathbf{u}}(i; x), u(i))$$

Condition 6 : Feasibility

There is at least a sequence that meets the constraints (in particular $x(0) \in X_0$ (the subset of state steerable in N steps to X_f with bounded controls in \mathbb{U}).

To summarize

The system $x^+ = f(x, u)$

The cost function $F(x(N)) + \sum_{i=0}^N L(x(i), u(i))$

- 1) f, L, L are continuous.
- 2) \mathbb{U} is compact, \mathbb{X} and $X_f \subset \mathbb{X}$ are closed.
- 3) $\{L(x, u) \rightarrow 0\} \Rightarrow \{x \rightarrow 0\}$
- 4) X_f is positively invariant (with some $\kappa_f(\cdot)$).
- 5) $F(\cdot)$ is a Lyapunov function under $\kappa_f(\cdot)$.
- 6) $x(0) \in X_N$.

How to choose X_f and $\kappa_f(\cdot)$?

- ① Infinite horizon $N = \infty$.

How to choose X_f and $\kappa_f(\cdot)$?

- ① Infinite horizon $N = \infty$.
- ② Point-wise final constraint $X_f = \{0\}$.

How to choose X_f and $\kappa_f(\cdot)$?

- ① Infinite horizon $N = \infty$.
- ② Point-wise final constraint $X_f = \{0\}$.
- ③ If the linearized system at 0 is stabilizable, then

How to choose X_f and $\kappa_f(\cdot)$?

- ① Infinite horizon $N = \infty$.
- ② Point-wise final constraint $X_f = \{0\}$.
- ③ If the linearized system at 0 is stabilizable, then
 - $\kappa_f(x) = -Kx$

How to choose X_f and $\kappa_f(\cdot)$?

- ➊ Infinite horizon $N = \infty$.
- ➋ Point-wise final constraint $X_f = \{0\}$.
- ➌ If the linearized system at 0 is stabilizable, then
 - $\kappa_f(x) = -Kx$
 - $(A - BK)^T P(A - BK) - P = -Q$ for some $P, Q > 0$

How to choose X_f and $\kappa_f(\cdot)$?

- ① Infinite horizon $N = \infty$.
- ② Point-wise final constraint $X_f = \{0\}$.
- ③ If the linearized system at 0 is stabilizable, then
 - $\kappa_f(x) = -Kx$
 - $(A - BK)^T P(A - BK) - P = -Q$ for some $P, Q > 0$
 - X_f is a level set of $x^T Px$, namely

$$X_f = \left\{ x \mid x^T Px \leq \varrho \right\}$$

for a sufficiently small $\varrho > 0$.

Example

$$\begin{aligned}x_1^+ &= x_1 + (1 + x_2^2)u \\x_2^+ &= \frac{3}{2}x_2 - x_1 e^u\end{aligned}$$

- ✓ Open-loop instable.
- ✓ The set of equilibrium states is given by

$$\mathcal{E}_{st} = \left\{ x^{(\alpha)} := \begin{pmatrix} \alpha \\ 2\alpha \end{pmatrix} ; \quad \alpha \in \mathbb{R} \right\}$$

Control objective starting at $x^{(0)} = (0, 0)$, stabilize the system around $x^{(1)} = (1, 2)$.

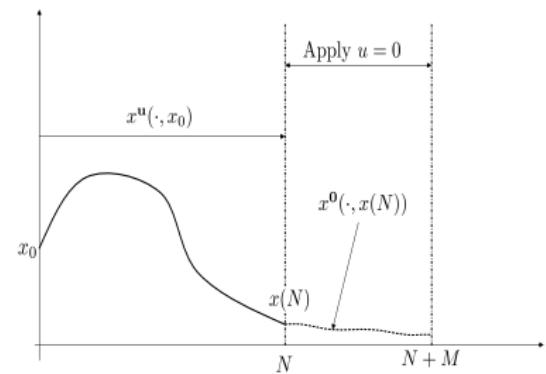
Consider the cost function

$$V(x, \mathbf{u}) := F(x(N)) + \sum_{i=0}^N L(x(i), u(i))$$

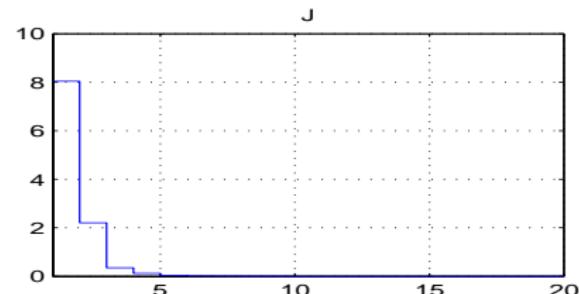
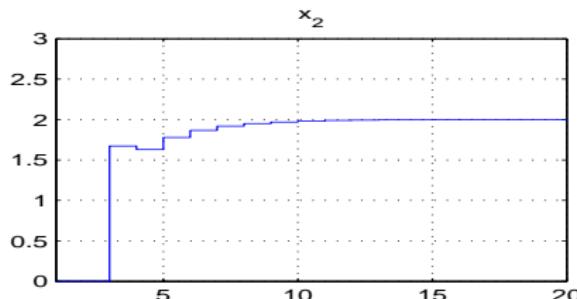
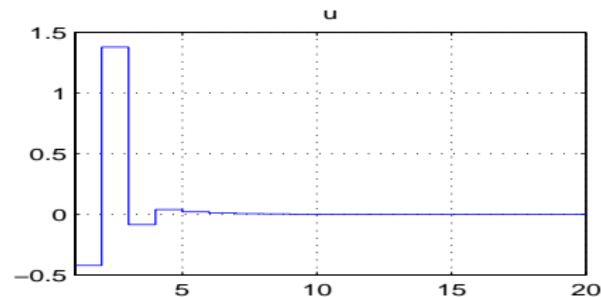
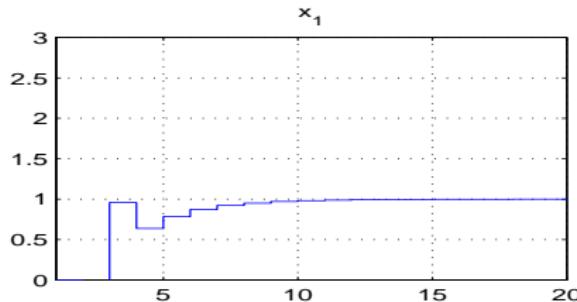
where

$$L(x, u) := \|x - x^{(1)}\|^2 + ru^2$$

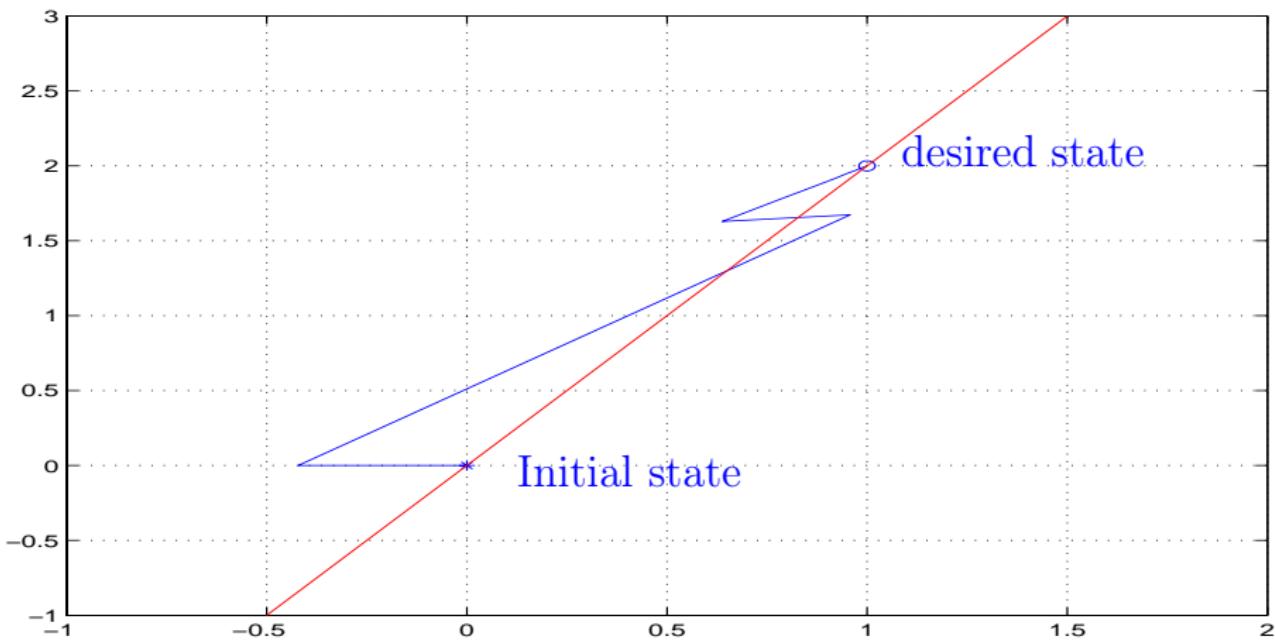
$$F(x) = \sum_{i=1}^{M-N} x^0(i; x)$$



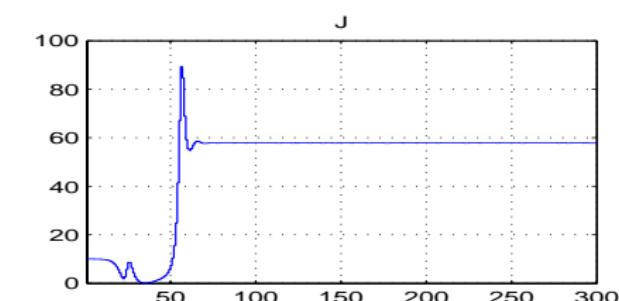
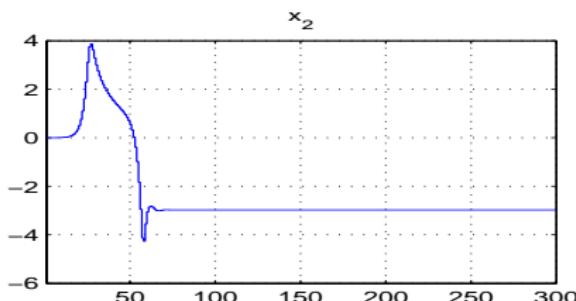
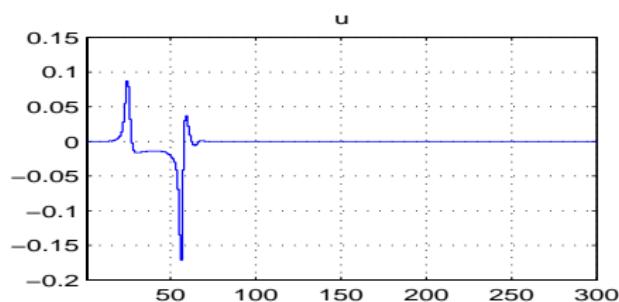
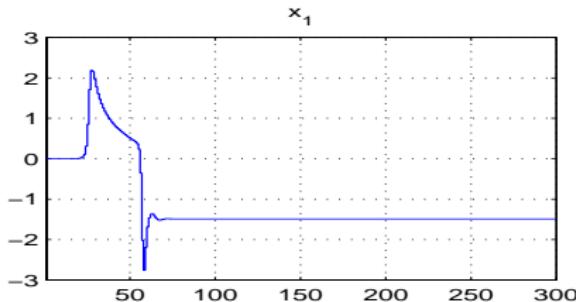
Test 1 : $N = 2$, $M = 2$, $r = 1$



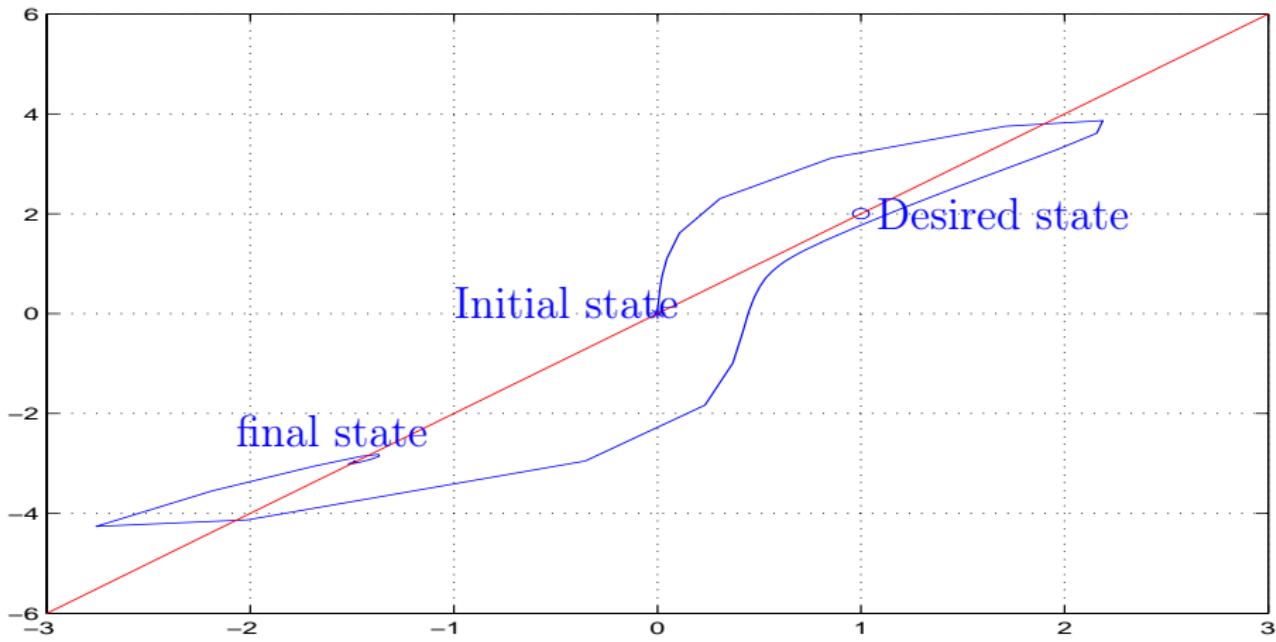
Test 1 : $N = 2, M = 2, r = 1$

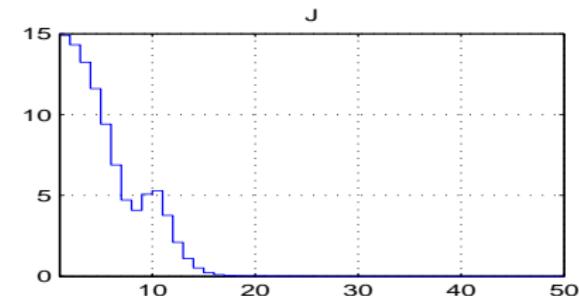
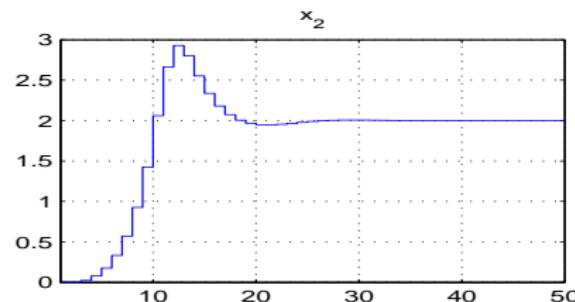
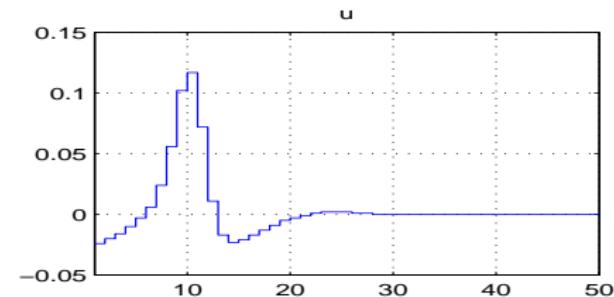
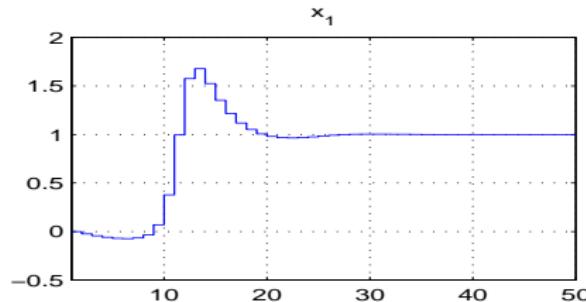


Test 2 : $N = 2$, $M = 2$, $r = 160$

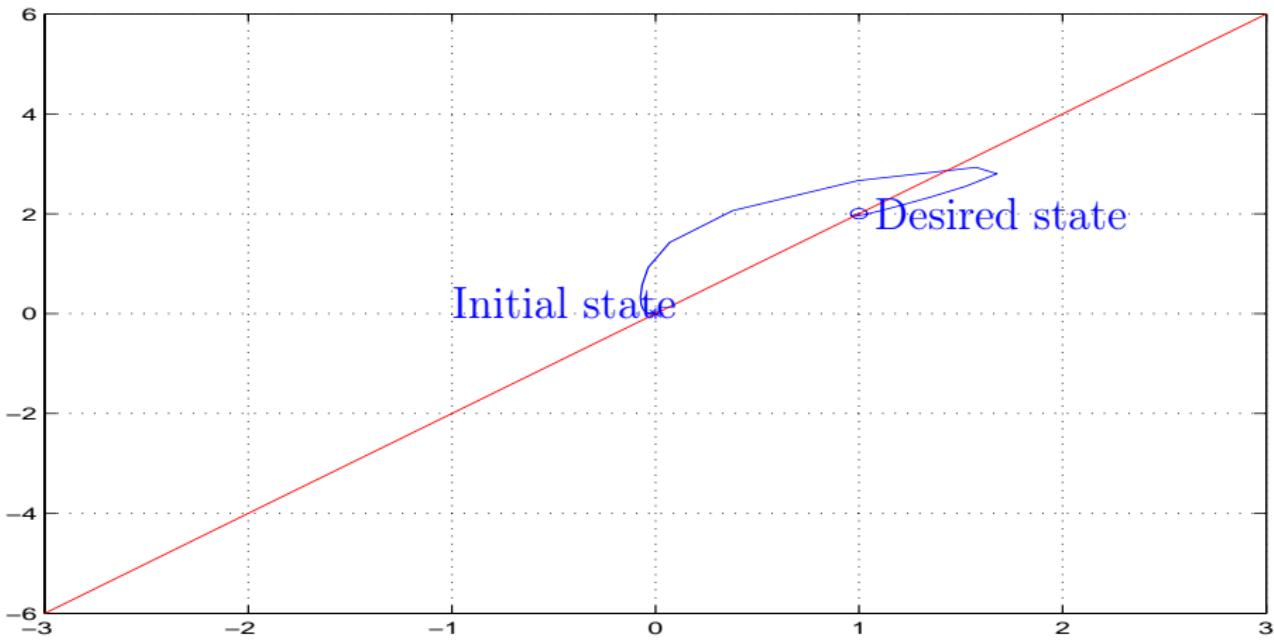


Test 2 : $N = 2, M = 2, r = 160$



Test 3 : $N = 2$, $M = 3$, $r = 160$ 

Test 3 : $N = 2, M = 3, r = 160$

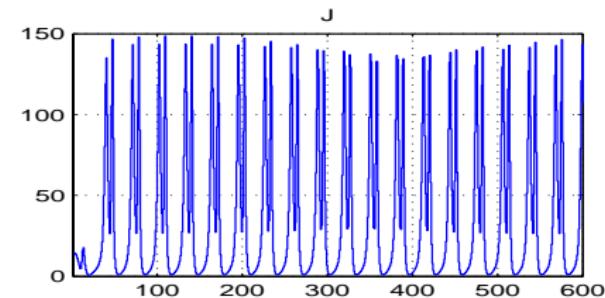
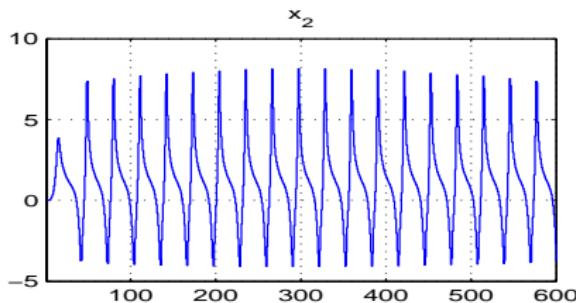
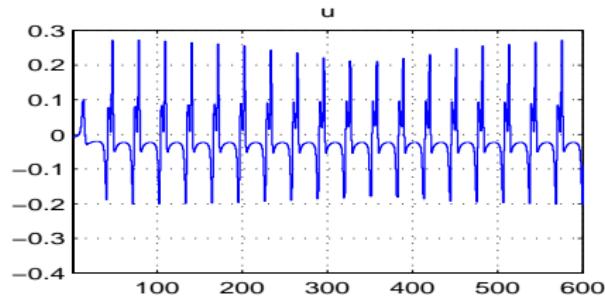
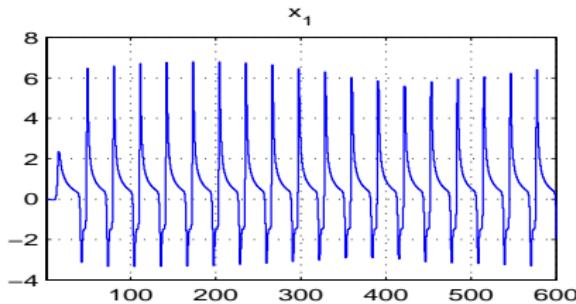


Increasing M enabled the target state to be reached.

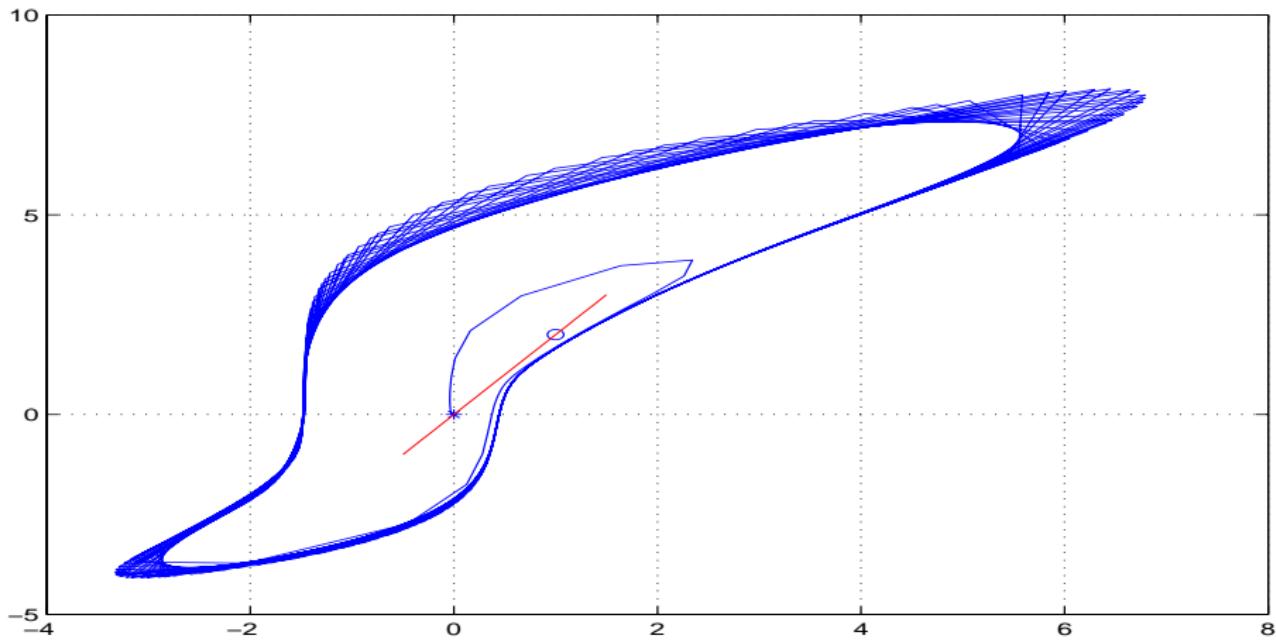
However, the control is again above 0.1,

So let us increase r again by taking

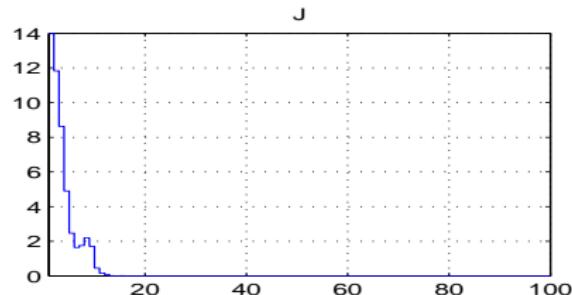
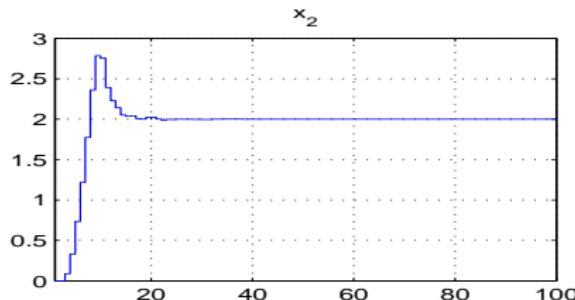
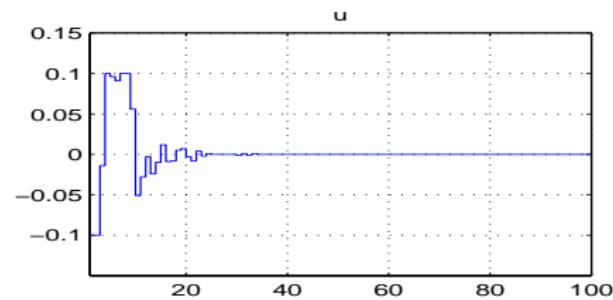
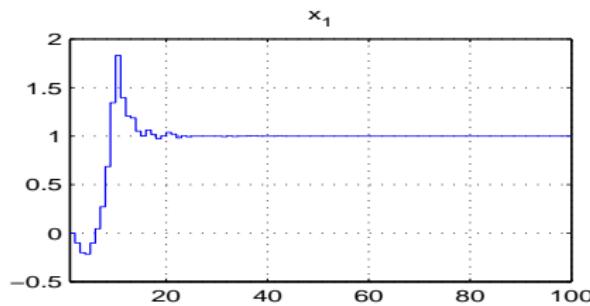
$$r = 500$$

Test 4 : $N = 2, M = 3, r = 500$ 

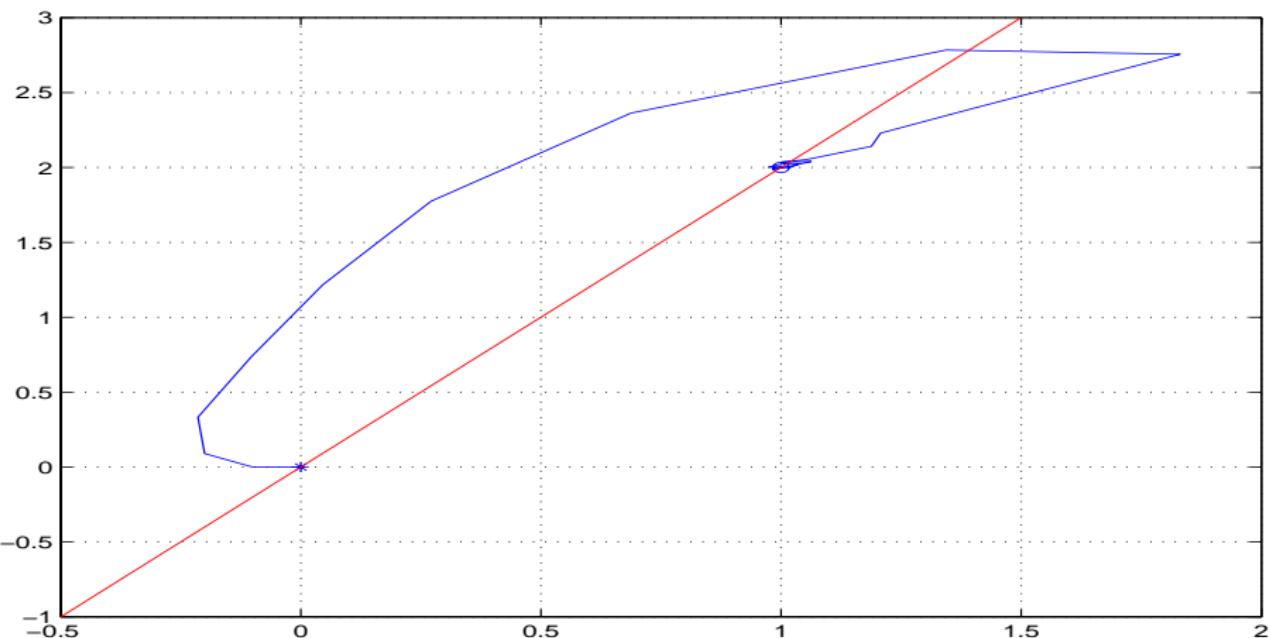
Test 4 : $N = 2$, $M = 3$, $r = 500$



Test 5 : $N = 3$, $M = 3$, $r = 1$, explicit constraint $|u| \leq 0.1$



Test 5 : $N = 3$, $M = 3$, $r = 1$, explicit constraint $|u| \leq 0.1$



The example shows that

- Nonlinear Model Predictive Control is a "*generic*" solution.

(Who remember the system's equations ?!!)

```
subroutine syst(x,u,xplus)
    implicit none
    double precision :: x(2), u, xplus(2)
    xplus(1)=x(1)+(1.0d0+x(2)**2)*u
    xplus(2)=1.5*x(2)-x(1)*dexp(u)
end subroutine syst
```

```
subroutine syst_long(x0,nu,ns,utilde,xtilde)
    implicit none
    external syst
    integer :: nu, ns, i
    double precision :: x0(2), utilde(nu), xtilde(ns+1,2)
    xtilde(1,:)=x0
    do i=1,nu
        call syst(xtilde(i,:),utilde(i),xtilde(i+1,:))
    enddo
    do i=nu+1,ns
        call syst(xtilde(i,:),0.0d0,xtilde(i+1,:))
    enddo
end subroutine syst_long
```

```
subroutine criterie(nu,utililde,J)
  use param
  use imsl
  implicit none
  integer :: nu, i
  double precision :: utililde(nu), J, xtilde(M+1,2)
  double precision :: dx(2)
  call syst_long(x0_glob,nu,M,utililde,xtilde)
  J=0.d0
  do i=1,nu
    J=J+qu*dabs(utililde(i))**2
    dx = xtilde(i+1,:)-xd_glob
    J=J+qx*dot_product(dx,eye(2).x.dx)
  enddo
  do i=nu+1,M
    dx = xtilde(i+1,:)-xd_glob
    J = J+qx*dot_product(dx,eye(2).x.dx)
  enddo
end subroutine criterie
```

Computation of the optimal sequence

```
subroutine uhat(x0,xd,nu,utilde,J)
use param
implicit none
external criter
integer :: nu, maxfcn=100
double precision :: x0(2), xd(2), utilde(nu), J
double precision :: utilde_guess(nu), ulb(nu), uub(nu)
x0_glob=x0; xd_glob=xd; utilde_guess=0.0d0
ulb=-umax; uub=umax
call dbcpol(criter,nu,utilde_guess,0,ulb,uub,1.0d-8,maxfcn,utilde,J)
end subroutine uhat
```

The example shows that

- Nonlinear Model Predictive Control is a "*generic*" solution.

The example shows that

- Nonlinear Model Predictive Control is a "*generic*" solution.
- Easy handling of constraints

The example shows that

- Nonlinear Model Predictive Control is a "*generic*" solution.
- Easy handling of constraints
- The stability IS AN ISSUE

To summarize

The system $x^+ = f(x, u)$

The cost function $F(x(N)) + \sum_{i=0}^N L(x(i), u(i))$

- 1) f, L, L are continuous.
- 2) \mathbb{U} is compact, \mathbb{X} and $X_f \subset \mathbb{X}$ are closed.
- 3) $\{L(x, u) \rightarrow 0\} \Rightarrow \{x \rightarrow 0\}$
- 4) X_f is positively invariant (with some $\kappa_f(\cdot)$).
- 5) $F(\cdot)$ is a Lyapunov function under $\kappa_f(\cdot)$.
- 6) $x(0) \in X_N$.

A PRELIMINARY EXAMPLE

Consider the nonlinear system

$$\dot{x}_1 = x_2 \quad ; \quad \dot{x}_2 = x_1 u$$

and the "*candidate*" Lyapunov function

$$V(x) = \frac{1}{2} [x_1^2 + x_2^2]$$

Compute the derivative of V

$$\dot{V}(x) = x_1 x_2 (1 + u)$$

A PRELIMINARY EXAMPLE

Consider the nonlinear system

$$\dot{x}_1 = x_2 \quad ; \quad \dot{x}_2 = x_1 u$$

and the "*candidate*" Lyapunov function

$$V(x) = \frac{1}{2} [x_1^2 + x_2^2]$$

Compute the derivative of V

$$\dot{V}(x) = x_1 x_2 (1 + u)$$

For classical Lyapunov design

V is not a good choice

(singular surface $x_1 x_2 = 0$)

A PRELIMINARY EXAMPLE

Consider the nonlinear system

$$\dot{x}_1 = x_2 \quad ; \quad \dot{x}_2 = x_1 u$$

and the "*candidate*" Lyapunov function

$$V(x) = \frac{1}{2} [x_1^2 + x_2^2]$$

Compute the derivative of V

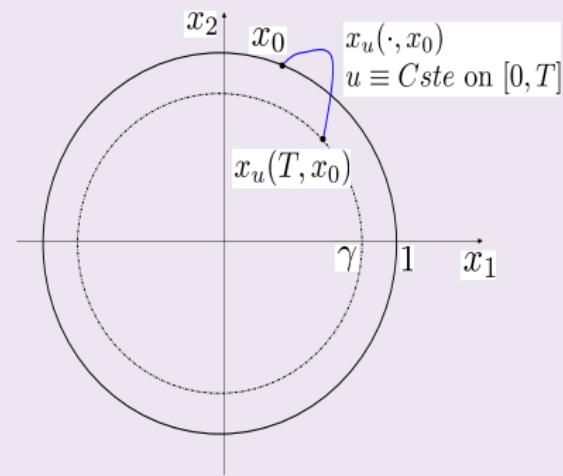
$$\dot{V}(x) = x_1 x_2 (1 + u)$$

For classical Lyapunov design

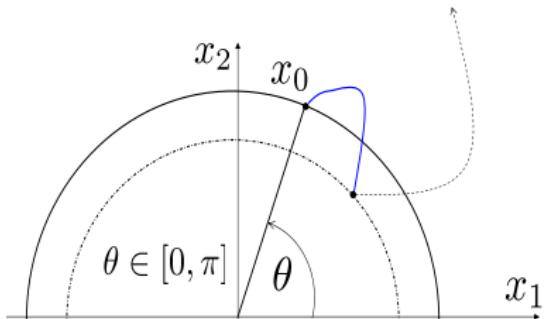
V is not a good choice

(singular surface $x_1 x_2 = 0$)

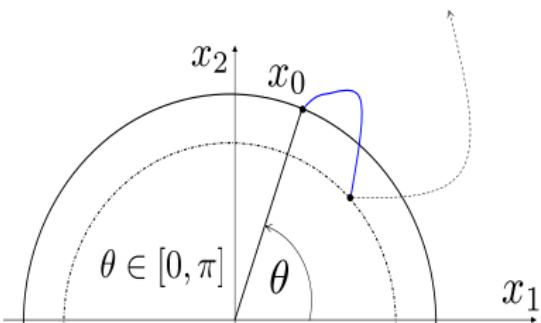
But...



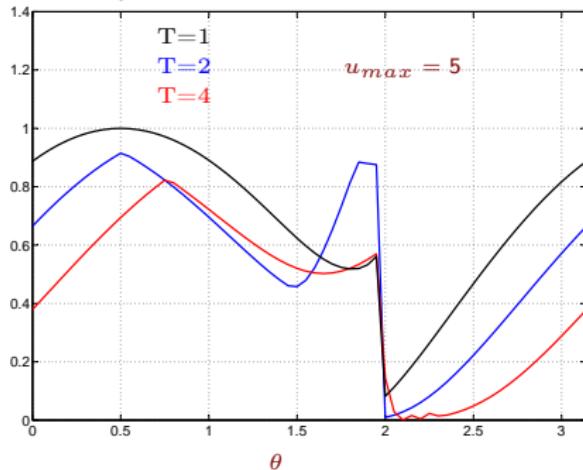
$$\min_{u(\cdot) \in u_0 \in [-u_{max}, +u_{max}]} \|x_u(T, x_0(\theta))\|$$



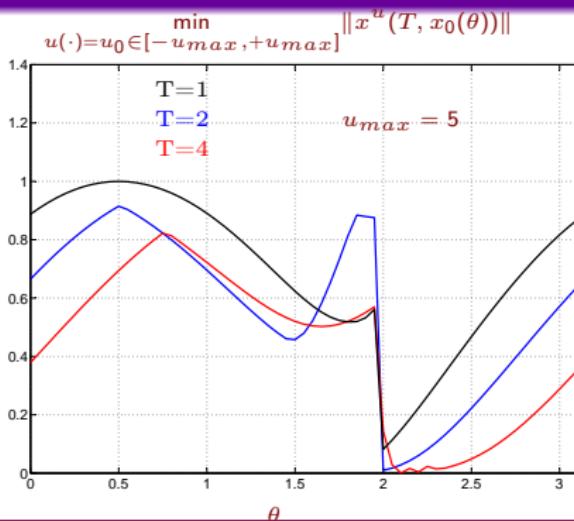
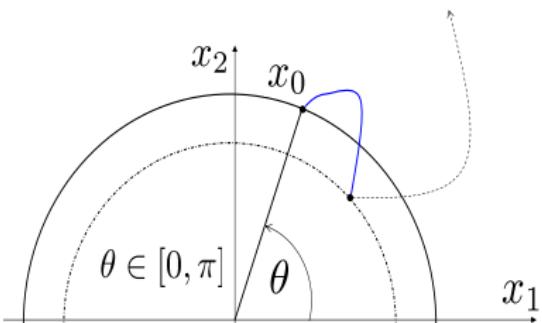
$$u(\cdot) \equiv u_0 \in [-u_{max}, +u_{max}] \quad \min \|x_u(T, x_0(\theta))\|$$



$$u(\cdot) = u_0 \in [-u_{max}, +u_{max}] \quad \min \|x^u(T, x_0(\theta))\|$$



$$u(\cdot) \equiv u_0 \in [-u_{max}, +u_{max}] \quad \min_{u(\cdot)} \|x_u(T, x_0(\theta))\|$$



To summarize : A long term contraction property

Whatever is the initial state $x_0 \in B(0, 1)$, there exists constant control $u \in [-5, +5]$ such that

$$V(x^u(2, x_0)) \leq 0.9 V(x_0) \quad \text{or} \quad [V(x^u(4, x_0)) \leq 0.82 V(x_0)]$$

A bad formulation

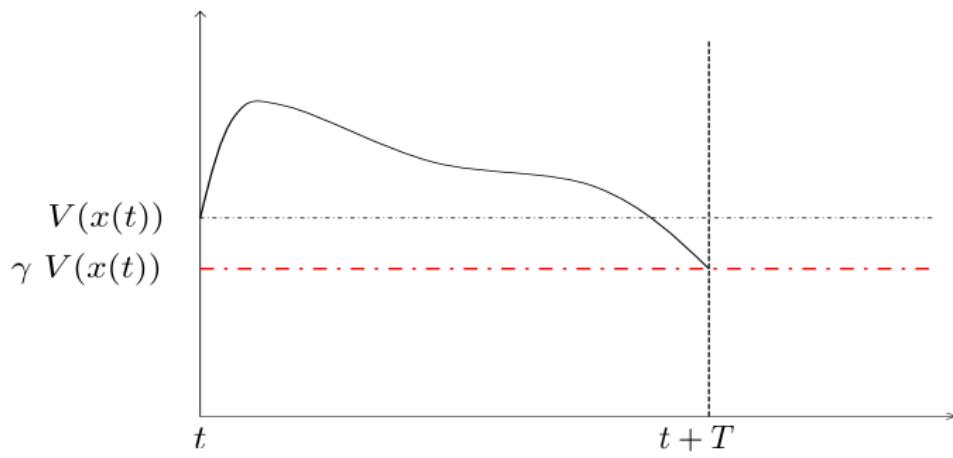
Define a receding horizon feedback based on the following open-loop optimization problem

$$\min_{\mathbf{u}(\cdot), \Delta \in [0, T]} \int_0^{\Delta} L(x_u(\tau, x(t))) d\tau \quad \text{under } V(x_u(t + \Delta, x(t))) \leq \gamma V(x(t))$$

A bad formulation

Define a receding horizon feedback based on the following open-loop optimization problem

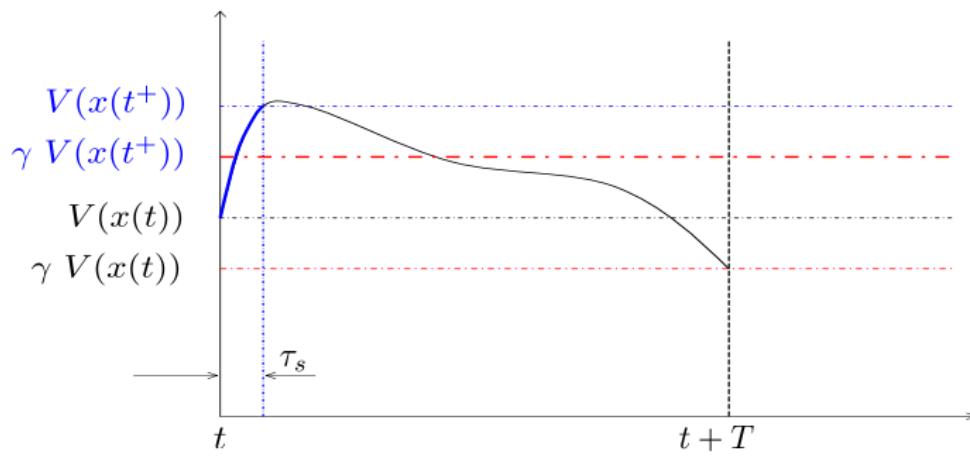
$$\min_{\mathbf{u}(\cdot), \Delta \in [0, T]} \int_0^{\Delta} L(x_u(\tau, x(t))) d\tau \quad \text{under } V(x_u(t + \Delta, x(t))) \leq \gamma V(x(t))$$



A bad formulation

Define a receding horizon feedback based on the following open-loop optimization problem

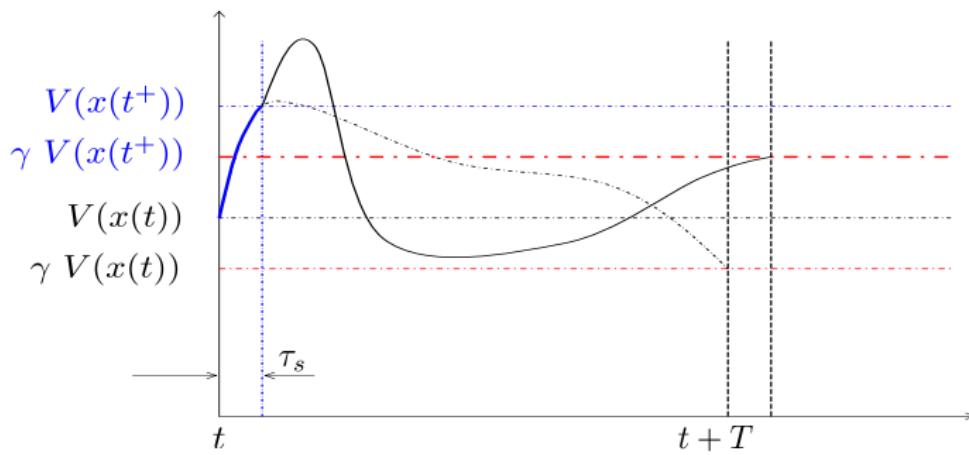
$$\min_{\mathbf{u}(\cdot), \Delta \in [0, T]} \int_0^\Delta L(x_u(\tau, x(t))) d\tau \quad \text{under } V(x_u(t + \Delta, x(t))) \leq \gamma V(x(t))$$



A bad formulation

Define a receding horizon feedback based on the following open-loop optimization problem

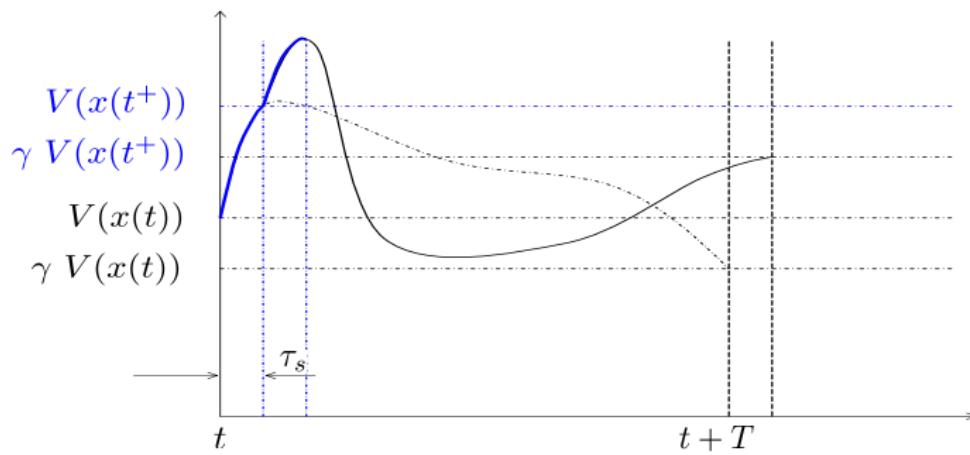
$$\min_{\mathbf{u}(\cdot), \Delta \in [0, T]} \int_0^\Delta L(x_u(\tau, x(t))) d\tau \quad \text{under } V(x_u(t + \Delta, x(t))) \leq \gamma V(x(t))$$



A bad formulation

Define a receding horizon feedback based on the following open-loop optimization problem

$$\min_{\mathbf{u}(\cdot), \Delta \in [0, T]} \int_0^\Delta L(x_u(\tau, x(t))) d\tau \quad \text{under } V(x_u(t + \Delta, x(t))) \leq \gamma V(x(t))$$



A bad formulation

Define a receding horizon feedback based on the following open-loop optimization problem

$$\min_{\mathbf{u}(\cdot), \Delta \in [0, T]} \int_0^{\Delta} L(x_u(\tau, x(t))) d\tau \quad \text{under } V(x_u(t + \Delta, x(t))) \leq \gamma V(x(t))$$

Updating systematically the contractive constraint

$$V(x_u(\Delta, x(t))) \leq \gamma V(x(t))$$

May cause instability in closed-loop

Kothare, S. L. de Oliveira and Morari, M. IEEE-TAC Vol 45 pp 1053-1071 (2000)

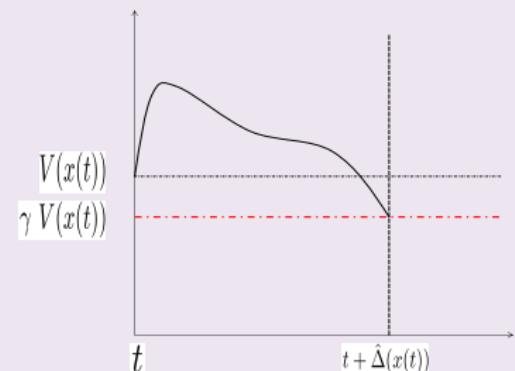
Kothare, S. L. de Oliveira and Morari, M. IEEE-TAC Vol 45 pp 1053-1071 (2000)

Either

Use the open-loop control

$$\hat{u}(\cdot, x(t))$$

on $[t, t + \hat{\Delta}(x(t))]$



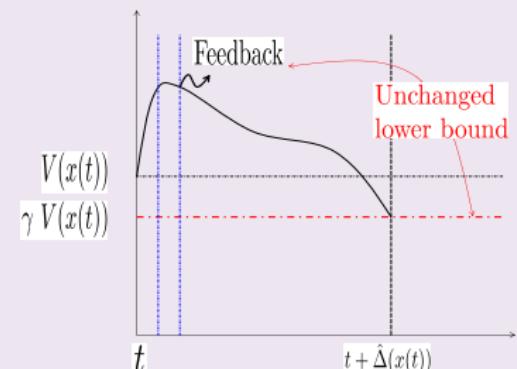
Kothare, S. L. de Oliveira and Morari, M. IEEE-TAC Vol 45 pp 1053-1071 (2000)

Or

Memorize $x(t)$ and use

$$V(x_u(\Delta, x(t + k\tau_s))) \leq \gamma V(x(t))$$

in a RH scheme during the time interval $[t, t + \hat{\Delta}(x(t))]$

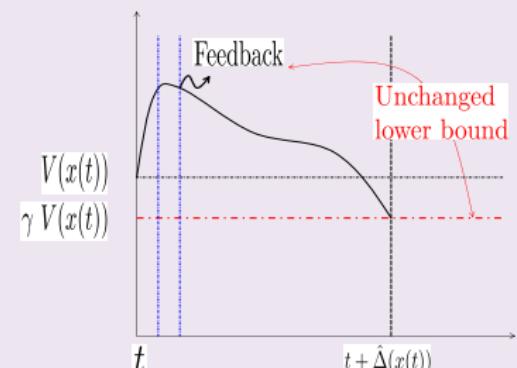


Kothare, S. L. de Oliveira and Morari, M. IEEE-TAC Vol 45 pp 1053-1071 (2000)

Or

Memorize $x(t)$ and use

$$V(x_u(\Delta, x(t + k\tau_s))) \leq \gamma V(x(t))$$

in a RH scheme during the time interval $[t, t + \hat{\Delta}(x(t))]$ 

- Non standard RH implementation
- Lack of reactivity
- Potential feasibility problems
 - In presence of disturbances
 - Under truncated optimization

Consider nonlinear systems

$$\dot{x} = f(x, u) \quad ; \quad x \in \mathbb{R}^n \quad ; \quad u \in \mathbb{R}^m \quad ; \quad f \text{ continuous}$$

satisfying the following assumption

Infinitely fast state excursions need infinite control

Consider nonlinear systems

$$\dot{x} = f(x, u) \quad ; \quad x \in \mathbb{R}^n \quad ; \quad u \in \mathbb{R}^m \quad ; \quad f \text{ continuous}$$

satisfying the following assumption

Infinitely fast state excursions need infinite control

For all finite horizon $T > 0$,

$$\lim_{\|x_0\| \rightarrow \infty} \left[\min_{\mathbf{u} \in \mathbb{W}^{[0,T]}} \min_{t \in [0,T]} \|F(t, x_0, \mathbf{u})\| \right] = \infty$$

for all compact subset $\mathbb{W} \subset \mathbb{R}^m$.

b

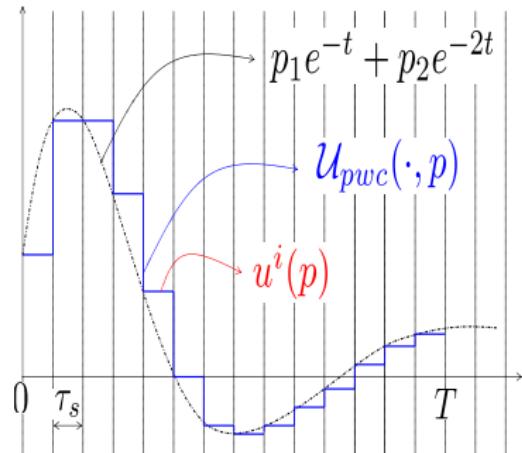
- ✓ Choose a sampling period τ_s
- ✓ Define a τ_s -piece-wise constant control profile

$$\mathcal{U}_{pwc}(\cdot, p) \quad ; \quad p \in \mathbb{P}$$

- ✓ The parametrization is called "*translatable*" if for all $p \in \mathbb{P}$, there is $p^+ \in \mathbb{P}$ s.t.

$$u^i(p^+) = u^{i+1}(p)$$

$$\forall i \in \{1, \dots, N-1\}$$



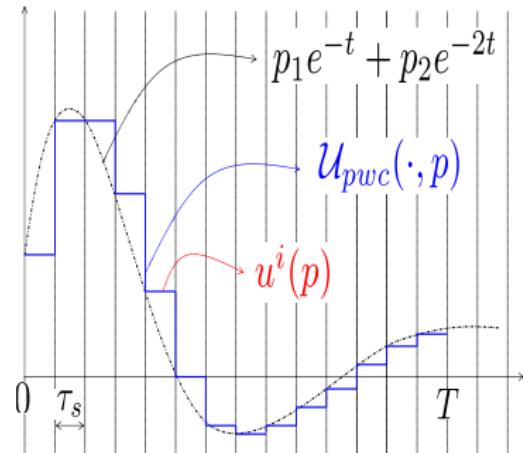
- ✓ Choose a sampling period τ_s
- ✓ Define a τ_s -piece-wise constant control profile

$$\mathcal{U}_{pwc}(\cdot, p) \quad ; \quad p \in \mathbb{P}$$

- ✓ The parametrization is called "*translatable*" if for all $p \in \mathbb{P}$, there is $p^+ \in \mathbb{P}$ s.t.

$$u^i(p^+) = u^{i+1}(p)$$

$$\forall i \in \{1, \dots, N-1\}$$



$$p^+ = \begin{pmatrix} e^{-\tau_s} & 0 \\ 0 & e^{-2\tau_s} \end{pmatrix} p$$

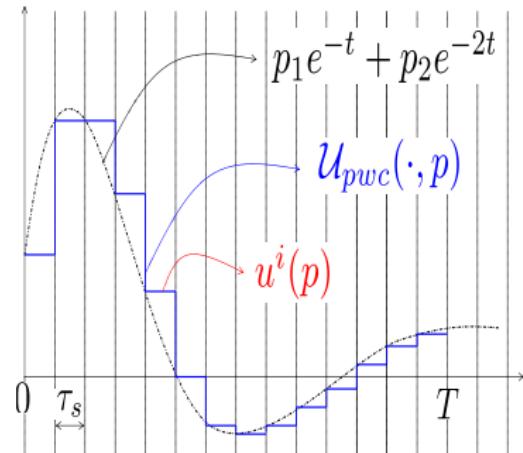
- ✓ Choose a sampling period τ_s
- ✓ Define a τ_s -piece-wise constant control profile

$$\mathcal{U}_{pwc}(\cdot, p) \quad ; \quad p \in \mathbb{P}$$

- ✓ The parametrization is called "*translatable*" if for all $p \in \mathbb{P}$, there is $p^+ \in \mathbb{P}$ s.t.

$$u^i(p^+) = u^{i+1}(p)$$

$$\forall i \in \{1, \dots, N-1\}$$



Notation $F(\cdot, x, p), V(\cdot, x, p)$

$$p^+ = \begin{pmatrix} e^{-\tau_s} & 0 \\ 0 & e^{-2\tau_s} \end{pmatrix} p$$

The strong contraction property

- ① $\exists \gamma \in]0, 1[$ s.t. for all x , there exists $p^c(x) \in \mathbb{P}$ such that

$$\min_{q \in \{1, \dots, N\}} V(q\tau_s, x, p^c(x)) \leq \gamma V(x)$$

The strong contraction property

- ① $\exists \gamma \in]0, 1[$ s.t. for all x , there exists $p^c(x) \in \mathbb{P}$ such that

$$\min_{q \in \{1, \dots, N\}} V(q\tau_s, x, p^c(x)) \leq \gamma V(x)$$

- ② $p_c(\cdot)$ is bounded over bounded sets

The strong contraction property

- ① $\exists \gamma \in]0, 1[$ s.t. for all x , there exists $p^c(x) \in \mathbb{P}$ such that

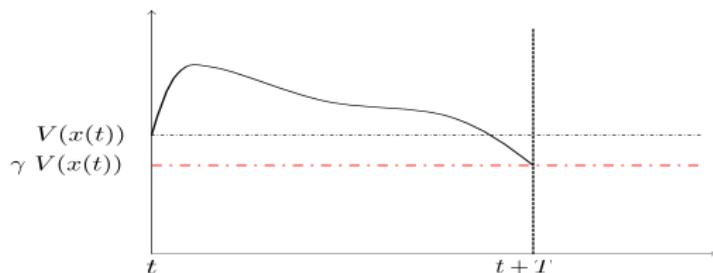
$$\min_{q \in \{1, \dots, N\}} V(q\tau_s, x, p^c(x)) \leq \gamma V(x)$$

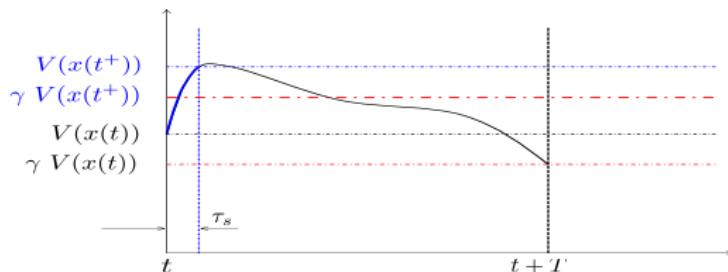
- ② $p_c(\cdot)$ is bounded over bounded sets
 ③ \exists a continuous function $\varphi : \mathbb{R}^n \rightarrow \mathbb{R}_+$ s.t. for all x :

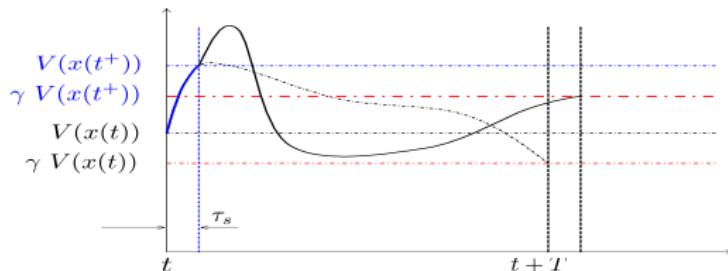
$$\|V_{1 \rightarrow N}(\cdot, x, p^c(x))\|_\infty \leq \varphi(x) \cdot V(x)$$

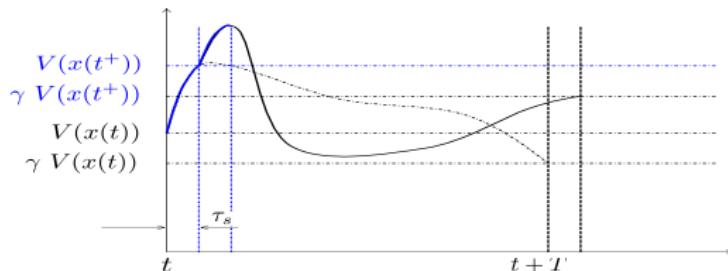
where

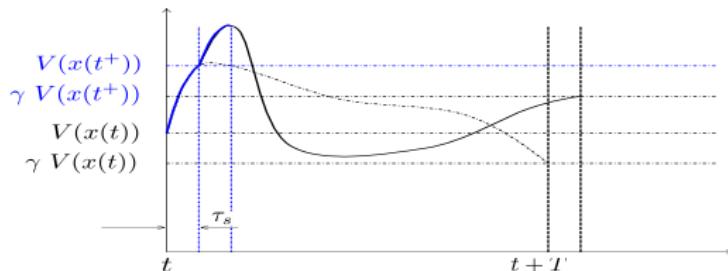
$$\|V_{1 \rightarrow q}(\cdot, x, p)\|_\infty = \max_{i \in \{1, \dots, q\}} V(i\tau_s, x, p)$$





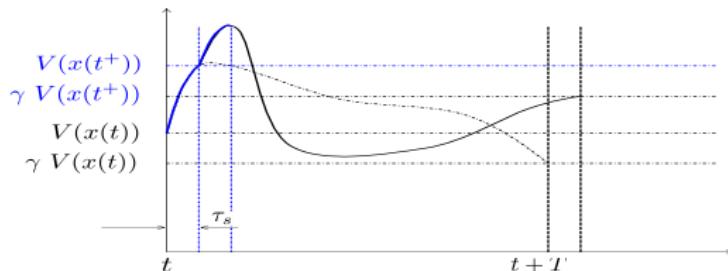






The open-loop optimal control problem

$$\min_{(q,p) \in \{1, \dots, N\} \times \mathbb{P}_{\mathbb{X}}} V(q\tau_s, x, p) + \alpha \frac{q}{N} \cdot \min\{\varepsilon^2, \|V_{1 \rightarrow q}(\cdot, x, p)\|_{\infty}\}$$

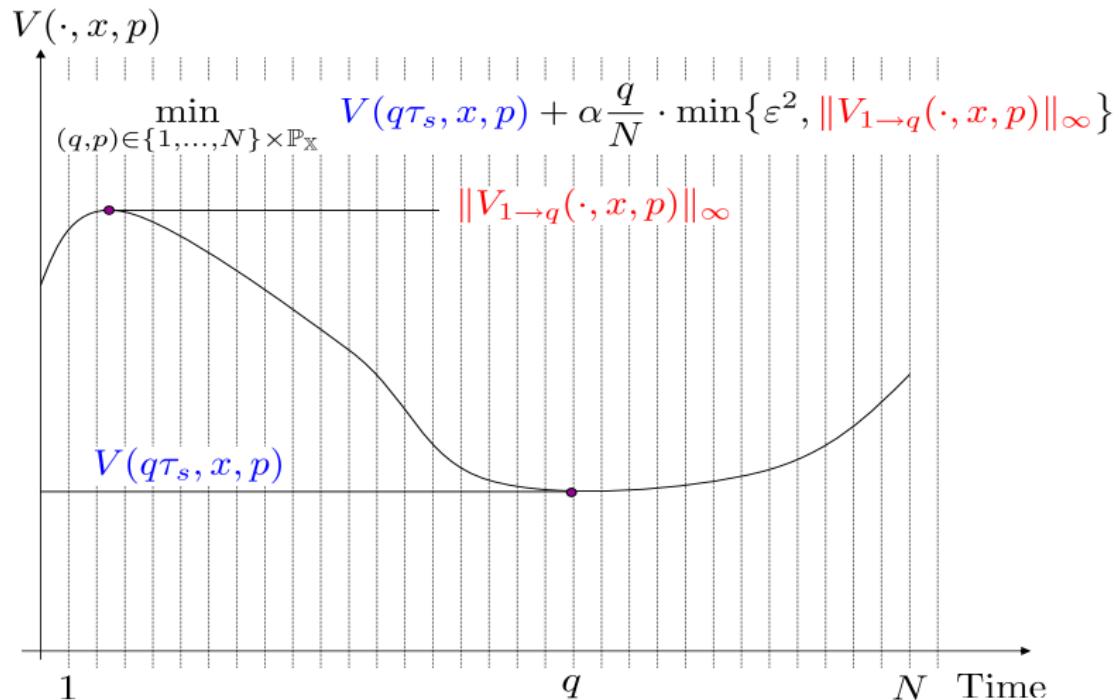


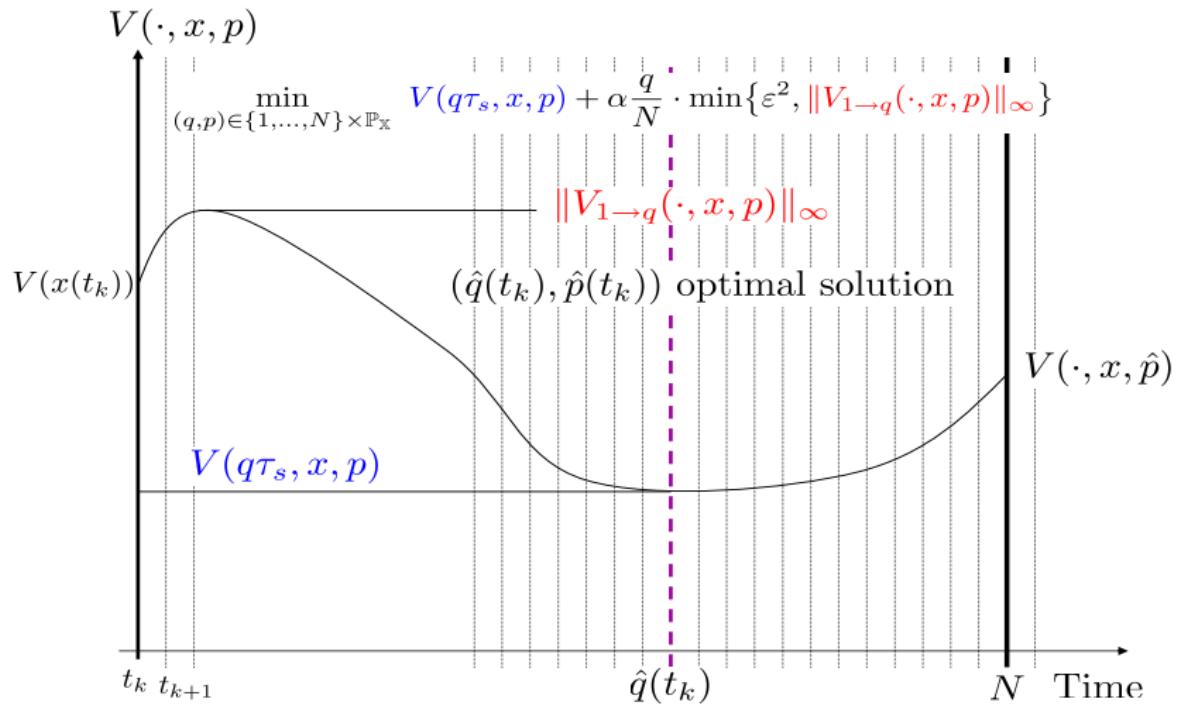
The open-loop optimal control problem

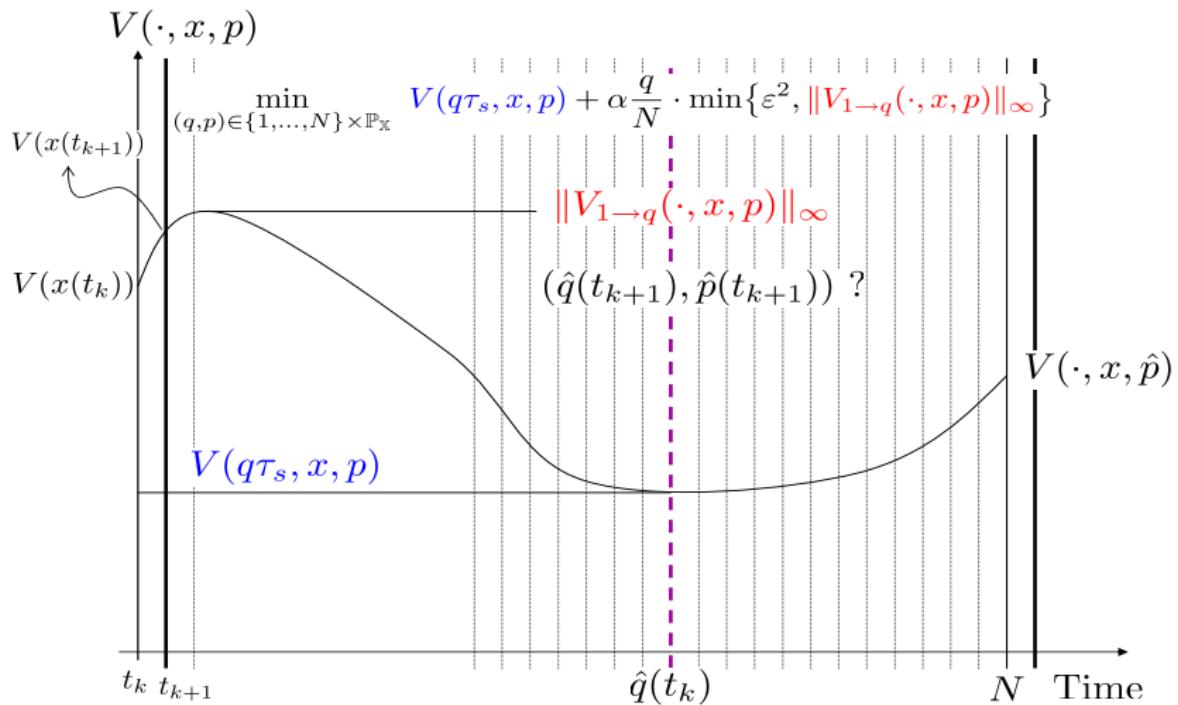
$$\min_{(q,p) \in \{1, \dots, N\} \times \mathbb{P}_{\mathbb{X}}} V(q\tau_s, x, p) + \alpha \frac{q}{N} \cdot \min\{\varepsilon^2, \|V_{1 \rightarrow q}(\cdot, x, p)\|_{\infty}\}$$

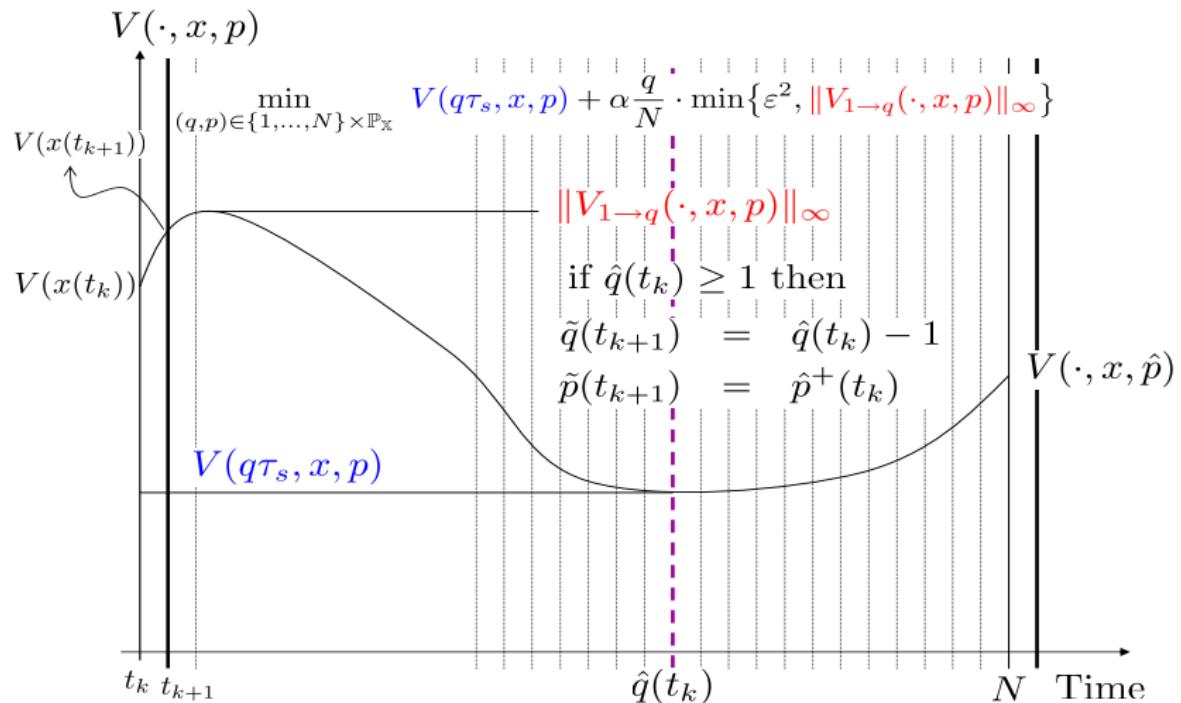
The receding-horizon state feedback

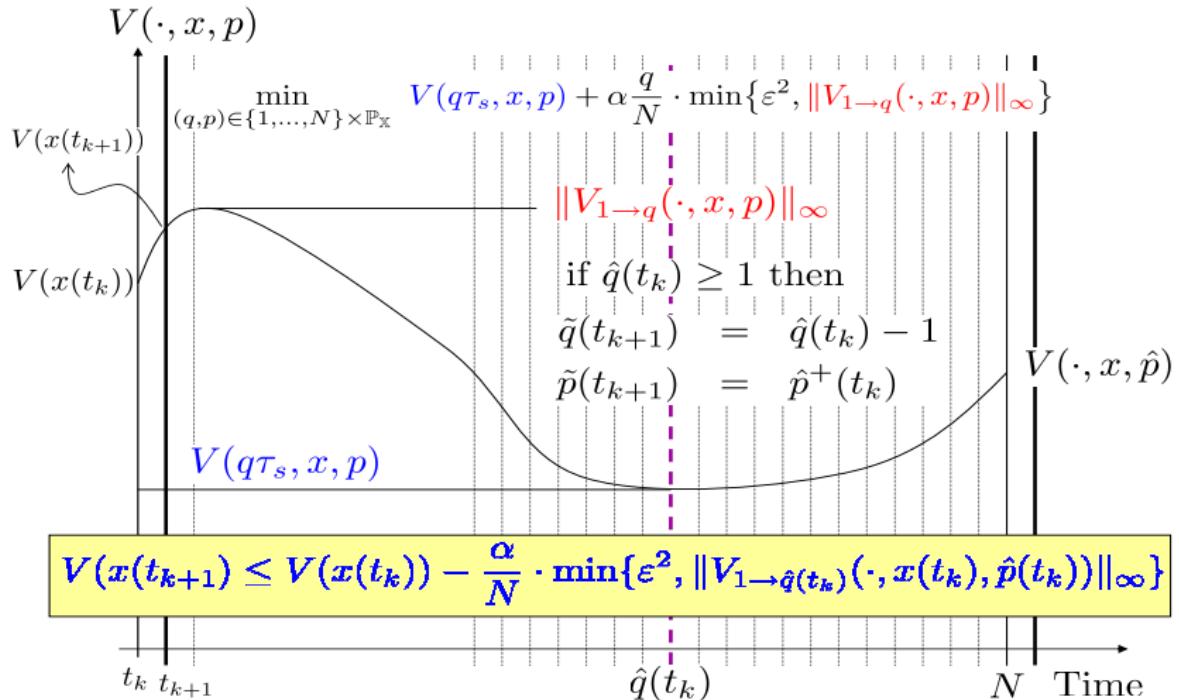
$$u(k\tau_s + \tau) = u^1(\hat{p}(x(k\tau_s))) \quad \forall \tau \in [0, \tau_s[$$











Basic Result

If the following conditions hold

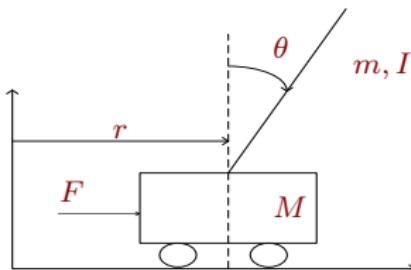
- ① Continuity (system/parametrization)
- ② Infinitely fast excursions need infinite controls
- ③ The control parametrization is translatable on

$$\mathbb{P}_{\mathbb{X}} := \mathbb{P} \cap B\left(0, \sup_{x \in \bar{B}(0, \rho(\mathbb{X}))} \|p^c(x)\| + \varepsilon_0\right) \subseteq \mathbb{P} \subseteq \mathbb{R}^{n_p}$$

Then, \exists sufficiently small $\varepsilon > 0$ and $\alpha > 0$ such that the RH feedback is well defined and makes the origin $x = 0$ asymptotically stable for the resulting CL dynamics with a region of attraction that contains \mathbb{X} .

Illustrative examples

The simple inverted pendulum : A self contained RH control



The system equations

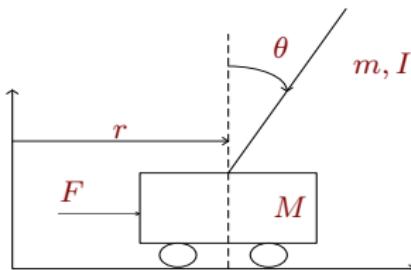
$$\begin{pmatrix} mL^2 + I & mL \cos \theta \\ mL \cos \theta & m + M \end{pmatrix} \begin{pmatrix} \ddot{\theta} \\ \ddot{r} \end{pmatrix} = \begin{pmatrix} mLg \sin \theta - k_\theta \dot{\theta} \\ F + mL\dot{\theta}^2 \sin \theta - k_x \dot{r} \end{pmatrix}$$

A pre-compensator

$$F = -K_{pre} \begin{pmatrix} r \\ \dot{r} \end{pmatrix} + u$$

Illustrative examples

The simple inverted pendulum : A self contained RH control

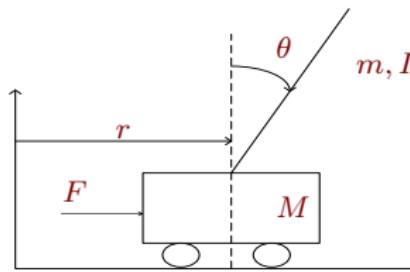


The system equations

$$\begin{aligned}\dot{x}_1 &= x_3 \quad ; \quad \dot{x}_2 = x_4 \\ \begin{pmatrix} \dot{x}_3 \\ \dot{x}_4 \end{pmatrix} &= [M(x)]^{-1} \begin{pmatrix} mLg \sin(x_1) - k_\theta \cdot x_3 \\ -K_{pre_1}x_2 - K_{pre_2}x_4 + mLx_3^2 \sin(x_1) - k_x x_4 + u \end{pmatrix}\end{aligned}$$

Illustrative examples

The simple inverted pendulum : A self contained RH control



Control parametrization

$$u^i(p) = p \cdot e^{-t_i/t_r} \quad ; \quad t_i = \frac{(i-1)\tau_s}{N}$$

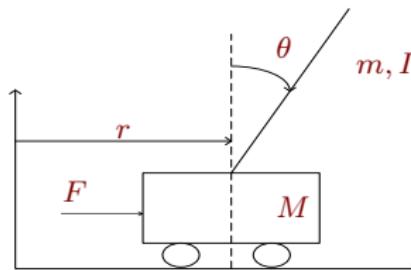
where $p \in \mathbb{P}(x) := [p_{min}(x), p_{max}(x)]$ s.t

$$p_{min}(x) = -F_{max} + K_{pre_1}x_2 + K_{pre_2}x_4$$

$$p_{max}(x) = +F_{max} + K_{pre_1}x_2 + K_{pre_2}x_4$$

Illustrative examples

The simple inverted pendulum : A self contained RH control



Use the contractive RH formulation given by :

$$V(x) = \frac{1}{2} [\dot{\theta}^2 + \beta r^2 + \dot{r}^2] + [1 - \cos(\theta)]^2$$

$$\min_{(q,p) \in \{1, \dots, N\} \times \mathbb{P}(x)} V(q\tau_s, x, p) + \frac{\alpha}{N} \cdot \min\{\varepsilon, \|V_{1 \rightarrow q}(\cdot, x, p)\|_\infty\}$$

$$u(k\tau_s + \tau) = u^1(\hat{p}(x(k\tau_s))) \quad \forall \tau \in [0, \tau_s[$$

Illustrative examples

The simple inverted pendulum : A self contained RH control

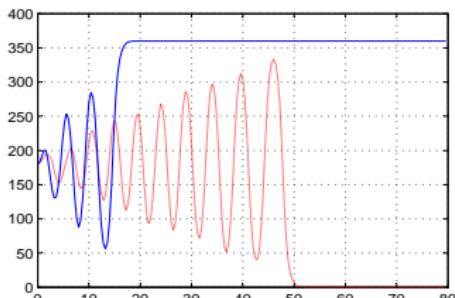
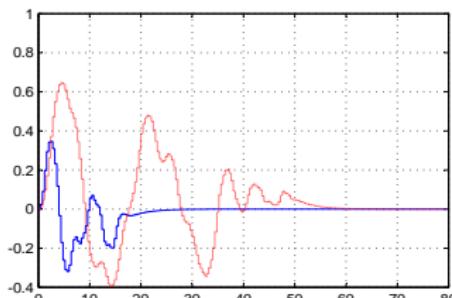
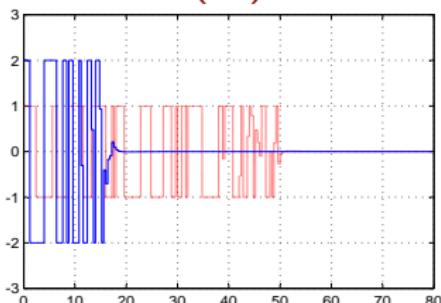
The parameters of the controller

| parameter | value | signification |
|------------------------|--------------------|---------------------------------|
| τ_s | 0.4 s | sampling period |
| N | 8 | horizon length |
| t_r | 0.2 | Constant for the control param. |
| $\alpha = \varepsilon$ | 0.01 | cost function parameters |
| K_{pre} | (2.5 10.0) | Pre-compensation gain |
| F_{max} | $\in \{1.0, 2.0\}$ | saturation level on F |
| β | $\in 10$ | weighting coefficient on r |

Runs on a 1.3 GHz Pentium-III

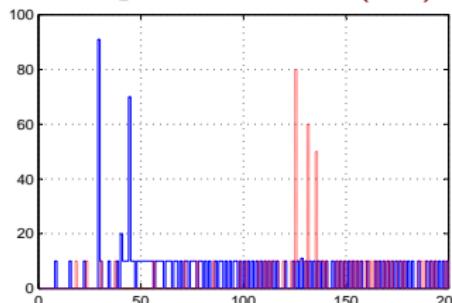
Illustrative examples

The simple inverted pendulum : A self contained RH control

 θ (deg) r (m) $F(N)$ 

Time (s)

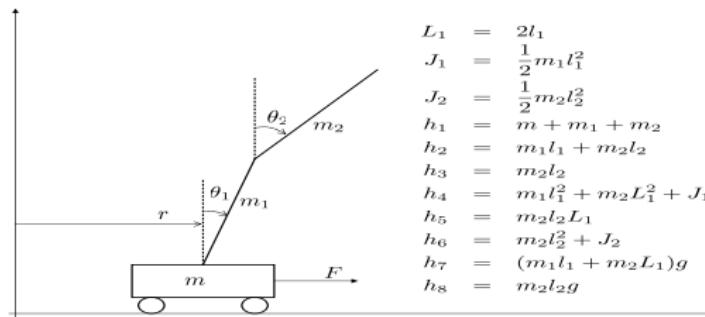
Computation time (ms)



Sampling periods

Illustrative examples

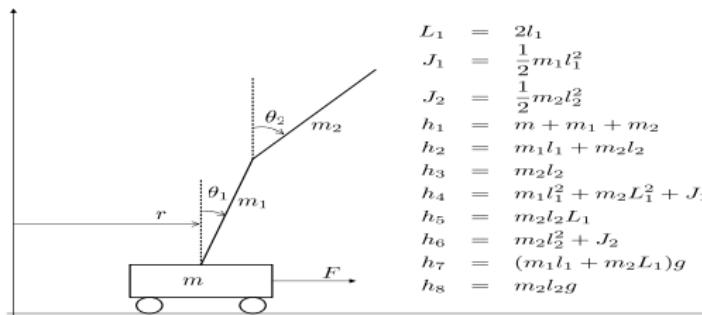
The double inverted pendulum : a hybrid control scheme



$$\begin{aligned}
 L_1 &= 2l_1 \\
 J_1 &= \frac{1}{2}m_1l_1^2 \\
 J_2 &= \frac{1}{2}m_2l_2^2 \\
 h_1 &= m + m_1 + m_2 \\
 h_2 &= m_1l_1 + m_2l_2 \\
 h_3 &= m_2l_2 \\
 h_4 &= m_1l_1^2 + m_2L_1^2 + J_1 \\
 h_5 &= m_2l_2L_1 \\
 h_6 &= m_2l_2^2 + J_2 \\
 h_7 &= (m_1l_1 + m_2L_1)g \\
 h_8 &= m_2l_2g
 \end{aligned}$$

Illustrative examples

The double inverted pendulum : a hybrid control scheme



$$\begin{aligned}
 L_1 &= 2l_1 \\
 J_1 &= \frac{1}{2}m_1l_1^2 \\
 J_2 &= \frac{1}{2}m_2l_2^2 \\
 h_1 &= m + m_1 + m_2 \\
 h_2 &= m_1l_1 + m_2l_2 \\
 h_3 &= m_2l_2 \\
 h_4 &= m_1l_1^2 + m_2L_1^2 + J_1 \\
 h_5 &= m_2l_2L_1 \\
 h_6 &= m_2l_2^2 + J_2 \\
 h_7 &= (m_1l_1 + m_2L_1)g \\
 h_8 &= m_2l_2g
 \end{aligned}$$

System equations

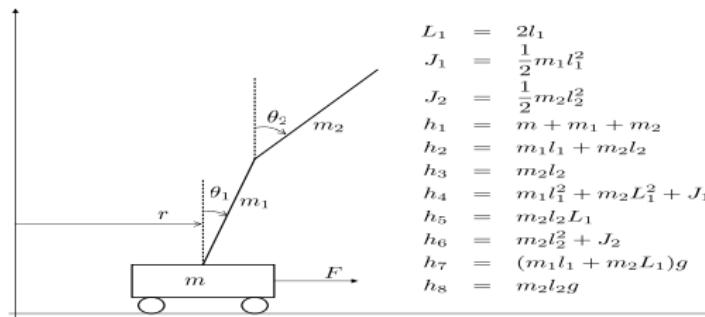
$$h_1\ddot{r} + h_2\ddot{\theta}_1 \cos \theta_1 + h_3\ddot{\theta}_2 \cos \theta_2 = h_2\dot{\theta}_1^2 \sin \theta_1 + h_3\dot{\theta}_2^2 \sin \theta_2 + F$$

$$h_2\ddot{r} \cos \theta_1 + h_4\ddot{\theta}_1 + h_5\ddot{\theta}_2 \cos(\theta_1 - \theta_2) = h_7 \sin \theta_1 - h_5\dot{\theta}_2^2 \sin(\theta_1 - \theta_2)$$

$$h_3\ddot{r} \cos \theta_2 + h_5\ddot{\theta}_1 \cos(\theta_1 - \theta_2) + h_6\ddot{\theta}_2 = h_5\dot{\theta}_1^2 \sin(\theta_1 - \theta_2) + h_8 \sin \theta_2$$

Illustrative examples

The double inverted pendulum : a hybrid control scheme

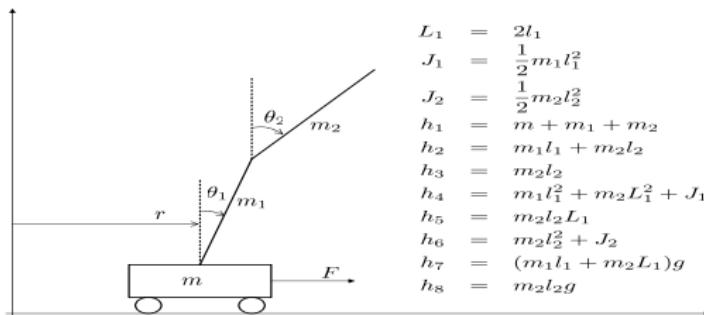


Pre-compensation

$$F = -K_{pre} \cdot \begin{pmatrix} r \\ \dot{r} \end{pmatrix} + u$$

Illustrative examples

The double inverted pendulum : a hybrid control scheme



Control parametrization

$$u^i(p) = p_1 \cdot e^{\lambda_1 t_i} + p_2 e^{-\lambda_2 t_i} \quad ; \quad t_i = \frac{(i-1)\tau_s}{N}$$

$$p_{min}(x) := \frac{1}{2} \left[-F_{max} + K_{pre} \begin{pmatrix} r \\ \dot{r} \end{pmatrix} \right] \quad ; \quad p_{max}(x) := \frac{1}{2} \left[+F_{max} + K_{pre} \begin{pmatrix} r \\ \dot{r} \end{pmatrix} \right]$$

The contractive RH controller

$$\begin{aligned}V(x) &= \frac{h_4}{2}\dot{\theta}_1^2 + \frac{h_6}{2}\dot{\theta}_2^2 + h_5\dot{\theta}_1\dot{\theta}_2 \cos(\theta_1 - \theta_2) + h_7[1 - \cos(\theta_1)] + \\&\quad + h_8[1 - \cos(\theta_2)] + h_1[r^2 + \dot{r}^2] \\u(k\tau_s + t) &= K_{RH}(x(k\tau_s)) := u^1(\hat{p}(x(k\tau_s))) \quad ; \quad t \in [0, \tau_s[\end{aligned}$$

The contractive RH controller

$$\begin{aligned} V(x) &= \frac{h_4}{2}\dot{\theta}_1^2 + \frac{h_6}{2}\dot{\theta}_2^2 + h_5\dot{\theta}_1\dot{\theta}_2 \cos(\theta_1 - \theta_2) + h_7[1 - \cos(\theta_1)] + \\ &\quad + h_8[1 - \cos(\theta_2)] + h_1[r^2 + \dot{r}^2] \\ u(k\tau_s + t) &= K_{RH}(x(k\tau_s)) := u^1(\hat{p}(x(k\tau_s))) \quad ; \quad t \in [0, \tau_s[\end{aligned}$$

A local LQR controller

$$K_L(x) = -L \cdot \begin{pmatrix} x_1^m \\ x_2^m \\ x_3 \\ \vdots \\ x_6 \end{pmatrix}$$

solving the discrete time Riccati equation

$$A_d^T S A_d - S - (A_d^T S B_d)(R + B_d^T S B_d^T)(B_d^T S A_d) + Q = 0$$

Hybrid controller for swing-up and stabilization of the double inverted pendulum

To summarize, the hybrid controller is given by

$$u(k\tau_s + \tau) = \begin{cases} K_{RH}(x(k\tau_s)) & \text{if } \|x(k\tau_s)\|_S^2 > \eta \\ K_L(x(k\tau_s)) & \text{otherwise} \end{cases}$$

Hybrid controller for swing-up and stabilization of the double inverted pendulum

To summarize, the hybrid controller is given by

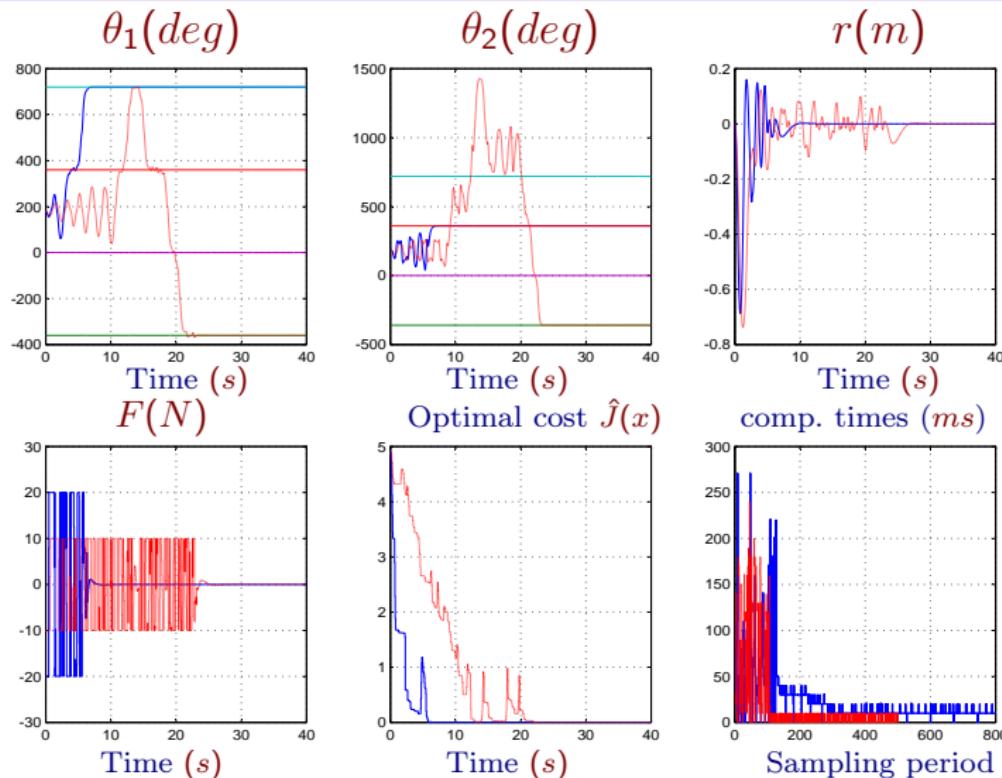
$$u(k\tau_s + \tau) = \begin{cases} K_{RH}(x(k\tau_s)) & \text{if } \|x(k\tau_s)\|_S^2 > \eta \\ K_L(x(k\tau_s)) & \text{otherwise} \end{cases}$$

The parameters of the controller

| parameter | value | signification |
|--------------------------|-----------|-----------------------------------|
| τ_s | 0.3 s | sampling period |
| N | 10 | horizon length |
| L | (360, 29) | (linear controller gain) |
| (λ_1, λ_2) | (100, 20) | Control parametrization |
| η | 1.0 | switching threshold |
| i_{max} | 20 | Max number of function evaluation |

Illustrative examples

The double inverted pendulum : a hybrid control scheme



Double inverted pendulum

le film

Illustrative examples

The double inverted pendulum : a hybrid control scheme

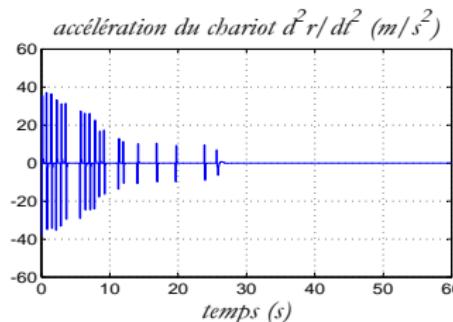
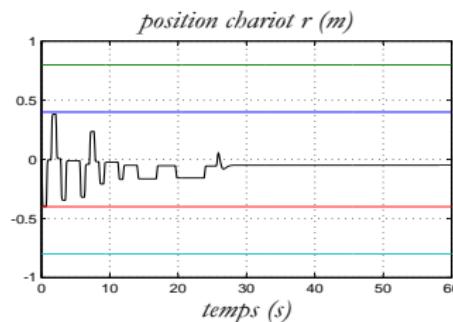
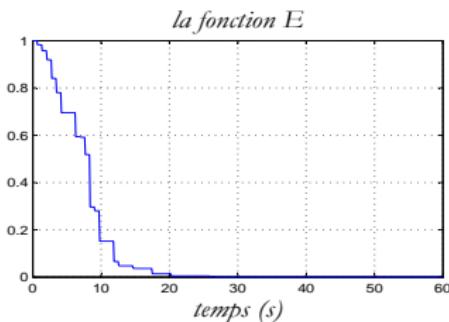
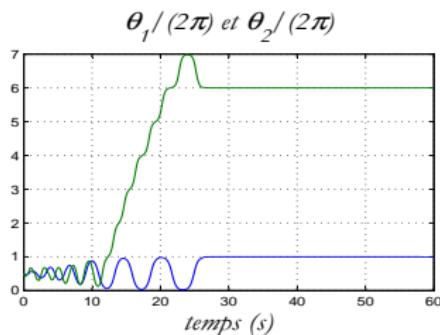
The twin pendulum

Movie

Illustrative examples

The double inverted pendulum : a hybrid control scheme

The twin pendulum



Illustrative examples

The double inverted pendulum : a hybrid control scheme

Nonlinear constrained NMPC for maximizing the production in polymerization processes.

Further readings

N. Marchand and M. Alamir

*Numerical stabilization of a **rigid spacecraft** with two actuators*

Journal of dynamic systems, measurements and control.

Vol 125, No 3, pp 489-491, (2003)

Further readings

M. Alamir and F. Boyer

Fast generation of attractive trajectories for an under-actuated satellite : Application to feedback control design

Journal of optimization in Engineering. Vol 4, pp 215-230,
(2003)

Further readings

M. Alamir

*Nonlinear Receding Horizon sub-optimal guidance law for minimum
interception time problem*

Control Engineering Practice. Vol 9, Issue 1, pp 107-116, (2001)

Further readings

M. Alamir and N. Marchand

Constrained Minimum Time Oriented Feedback Control For the Stabilization of Nonholonomic Systems in Chained Form

Journal of optimization Theory and Applications. Vol 118,
No 2, pp 229-244, (2003)

Further readings

A. Hably, N. Marchand and M. Almir

Constrained Minimum-Time Oriented Stabilization of Extended Chained Form Systems

CDC-ECC. Spain, (2005).

Further readings

M. alamir and H. Khennouf

*Discontinuous Receding Horizon Control Based Stabilizing Feedback
for Nonholonomic Systems in Power Form*

CDC. New Orleans, (1995).

Further readings

A. Chemori and M. Alamir

Limit Cycle Generation for a Class of Nonlinear Systems with jumps using a Low Dimensional Predictive Control

International Journal of Control. Vol 78, Issue 15, pp 1206-1217, (2005)

Further readings

A. Chemori and M. Alimir

Multi-step Limit Cycle Generation for Rabbit's Walking Based on a Nonlinear Low dimensional Predictive Control Scheme

International Journal of Mechatronics. To Appear (2005-6)

Further readings

M. Alamir, F. Ibrahim and J. P. Corriou

A Flexible Nonlinear Model Predictive Control Scheme for Quality/Performance Handling in Nonlinear SMB Chromatography

Journal of Process Control. To appear (2005)

Further readings

S. A. Attia, M. Alamir and C. Canudas de Wit

A Voltage Collapse Avoidance in Power Systems : A Receding Horizon Approach

International Journal on Intelligent automation and Soft Computing, Special Issue on “*Intelligent automation in power systems*”. To appear (2005)

Further readings

M. Alamir and G. Bornard

On the stability of receding horizon control of nonlinear discrete-time systems

Systems & Control Letters, Vol 23, pp 291-296, (1995).

Further readings

M. Alamir and N. marchand

Numerical Stabilization of Nonlinear Systems- Exact Theory and Approximate Numerical Implementation

European Journal of Control, Vol 5, pp 87-97, (1999).

Further readings

M. Alamir and G. Bornard

Stability of truncated Infinite Constrained Receding Horizon Scheme : The General Nonlinear Case

Automatica, Vol 31, No 9, pp 1353-1356, (1995).

Further readings

M. Alamir and I. Balloul

Robust Constrained Control Algorithm for General Batch Processes

International Journal of Control, Vol 72, No 14, pp 1271-1287,
(1999).

Further readings

M. Alamir

A new Path Generation Based Receding Horizon Formulation for Constrained Stabilization of Nonlinear Systems

Automatica, Vol 40, Issue 4, pp 647-652, (2004).

Further readings

M. Alamir

A Low Dimensional Contractive NMPC Scheme for Nonlinear Systems Stabilization : Theoretical Framework and Numerical Investigation on Relatively Fast Systems.

Workshop on Assessment and Future Directions of NMPC,
Freudenstadt, Germany (2005).

Illustrative examples

The double inverted pendulum : a hybrid control scheme

Download this presentation at

<http://www.lag.ensieg.inpg.fr/alamir/downloads.htm>